

PHASE 2 GROUND INVESTIGATION REPORT FOR OAKLEY FARM, PRIORS ROAD, CHELTENHAM, GLOS GL52 5AQ



PREPARED FOR ROBERT HITCHINS LIMITED











Report No. 4360/2



		Report Production Record							
Report No	4360/2	4360/2							
Site Name	Oakley Farm, Priors	Oakley Farm, Priors Road, Cheltenham, Gloucestershire GL52 5AQ							
Client	Robert Hitchins Lim	Robert Hitchins Limited							
Report on	Ground Investigatio	Ground Investigation							
Prepared by	Timothy D BSc(Hons) M	Coe Sc FGS							
Approved by	, David J W BSc(Geol) CGeo								
		Report Issue / Revision Record							
lssue No.	Date	Revision Details							
1	22 November 2018	Final							
	• • • • • • • • • • • • • • • • • • • •								

COPYRIGHT AND NON-DISCLOSURE NOTICE

The contents and layout of this report are subject to copyright owned by Wilson Associates (2018) save to the extent that copyright has been legally assigned by us to another party or is used by Wilson Associates under licence. To the extent that we own the copyright of this report, it may not be copied or used without our prior written agreement for any purpose other than the purpose indicated in this report.

The methodology (if any) contained in this report is provided to you in confidence and must not be disclosed or copied to third parties without the prior written agreement of Wilson Associates. Disclosure of that information may constitute an actionable breach of confidence or may otherwise prejudice our commercial interests. Any third party who obtains access to this report by any means will, in any event, be subject to the Third Party Disclaimer set out below.

THIRD PARTY DISCLAIMER

Any disclosure of this report to a third party is subject to this disclaimer. The report was prepared by Wilson Associates at the instruction of, and for use by, our client named on the front of the report. It does not in any way constitute advice to any third party who is able to access it by any means. Wilson Associates excludes to the fullest extent lawfully permitted all liability whatsoever for any loss or damage howsoever arising from reliance on the contents of this report. We do not however exclude our liability (if any) for personal injury or death resulting from our negligence, for fraud or any other matter in relation to which we cannot legally exclude liability. Legal re-assignment to another party can be arranged - please contact this Practice for further details.



CONTENTS

REPOF	RT		Page No.
1	INTRODUCTION		1
2	PROPOSED DEVELOPMENT		2
3	GROUND INVESTIGATION REPORT		2
	Site Works	2	
	Laboratory Testing – Geotechnical	3	
	Laboratory Testing - Contamination	6	
	Discussion on Ground Conditions	7	
	Percolation Testing – Soakaway Feasibility	9	
4	GEOTECHNICAL DESIGN REPORT		10
	Slope Stability	10	
	Foundation Design	11	
	Pavement Design	14	
	Material Suitability in Earthworks	14	
	Recommendations for Monitoring of Ground Conditions During Construction	15	
5	CONTAMINATION RISK ASSESSMENT AND SOIL WASTE CLASSIFICATION		15
	Human Health	15	
	Water Supply Pipework	17	
	Landfill & Radon Gas	18	
	Controlled Waters	19	
	Topsoil Suitability For Retention	19	
	Waste Classification For Offsite Disposal Of Arisings	20	
	Caveats	21	
6	REFINED CONCEPTUAL SITE MODEL		22
7	CONCLUSIONS AND RECOMMENDATIONS		23
8	REFERENCES		25



Job No. 4360/2 Page No. iv

DRAWINGS	No.
SITE LOCATION	4360/2/1
EXISTING SITE LAYOUT PLAN SHOWING INVESTIGATION LOCATIONS	4360/2/2

APPENDICES

- 1 BOREHOLE LOGS (INCLUDING PHOTOGRAPHS)
- 2 CONTAMINATION STATUTORY FRAMEWORK/METHODOLOGY AND CERTIFIED CONTAMINATION TEST RESULTS
- 3 BS3882:2015 TOPSOIL CERTIFICATES OF ANALYSIS
- 4 CERTIFIED GEOTECHNICAL TEST RESULTS
- 5 WASTE CLASSIFICATION REPORT AND WAC TEST RESULTS
- 6 GAS / WATER MONITORING RESULTS



PHASE 2 GROUND INVESTIGATION REPORT FOR OAKLEY FARM, PRIORS ROAD, CHELTENHAM, GLOUCESTERSHIRE GL52 5AQ PREPARED FOR ROBERT HITCHINS LIMITED

1 INTRODUCTION

- 1.1 The above site in Cheltenham is under consideration for a residential development. A ground investigation was requested in order to assess site suitability in respect of its contamination status and geotechnical conditions for appropriate foundation and ground floor slab design. This report follows on from a Phase 1 desk study (WA Report ref 4360) undertaken by this Practice in June 2018, to which reference should be made when reading this current report.
- **1.2** The Geo-environmental assessment has been carried out in accordance with BS10175:2011 "Code of Practice for the Investigation of Potentially Contaminated Sites" and EA document CLR 11 "Model Procedures for the Management of Land Contamination".
- 1.3 The geotechnical investigation has been carried out in general accordance with Eurocode 7 'Geotechnical Design', in particular BS EN 1997-1:2004 and 1997-2:2007 and BS EN ISO 14688-1:2002 and 14688-2:2004. The proposed development is considered to fall into the Geotechnical Category 2 classification, thus routine field and laboratory testing methods have been adopted. Reference has also been made to BS5930:2015 Code of Practice for Ground Investigations, and National House Building Council (NHBC) Standards Chapter 4.2 'Building Near Trees'.
- **1.4** This report has been prepared in accordance with email instruction from Edward Argent of Robert Hitchins Limited received on 18 July 2018. Reliance on this report is presently restricted to Robert Hitchins Limited.
- **1.5** In summary the previous desk study established that the site has remained undeveloped farmland with no history of industrial or other former usage, thus no no-site contamination sources are anticipated. It is underlain by clay/mudstone bedrock of the Charmouth Mudstone Formation (CMF) with no record of superficial deposits,



although given the sloping nature unrecorded landslip is a possibility. Off-site features may pose a risk of landfill gas migration onto site.

2 PROPOSED DEVELOPMENT

2.1 The site is being considered for a residential end use. No proposed development layout plan was available at the time of writing.

3 **GROUND INVESTIGATION REPORT**

Site Works

- **3.1** The Phase 2 intrusive investigation took place on 30-31 July 2018 by way of borehole drilling. The location of all exploratory hole positions were selected by this Practice (in conjunction with the Client) in order to obtain good spatial coverage across the site within the time available, and as requested positions were primarily focused on the southern half of the site. Positions were subsequently marked out on site (again by this Practice) using on and off-site reference points, and are indicated on drawing 4360/2/2. A CAT electrical service scanner was deployed prior to all intrusive works and as an added precaution (in light of recorded water pipework in the vicinity) boreholes WS10-11 were initiated by manually excavated inspection pits up to 1.0m depth. No services (recorded or unrecorded) were physically encountered during the intrusive works.
- **3.2** A total of eleven windowless sampling (small diameter) boreholes (WS1-11) were drilled to depths of up to 4.45m. Boreholes WS1-9 were drilled using an Archway Competitor Dart 338 windowless-sampling drilling rig and boreholes WS10-11 were drilled using a Terrier 2002 windowless-sampling drilling rig. The boreholes were logged on-site by a suitably qualified engineer from this Practice in accordance with Eurocode 7 (BS EN ISO 14688-1:2002 and 14688-2:2004), and representative disturbed samples taken for geotechnical and contamination testing as appropriate. In-situ cone penetration tests (CPT) or standard penetration tests (SPT) were completed at 1.0m intervals in accordance with BS EN ISO 22476-3:2005 to assess the relative density of the material penetrated and these results are indicated on the respective logs in Appendix 1.



- 3.3 Insitu percolation testing was undertaken during the works to establish the infiltration potential of the natural ground with 'falling head' percolation tests undertaken in BH's WS1 & 6. Results are presented graphically on the logs in Appendix 1 and soakaway feasibility is discussed in Section 3.21-3.22.
- **3.4** Following completion of logging and sampling, all boreholes except WS5, 7 and 9 were installed with standpipes and of those monitoring wells, five (WS1-2, WS4, WS6 and WS11) were also fitted with gas valves. Response zones are typically between 1.0m and 4.0m depth (1.0-3.0m depth in WS10), as shown on the respective borehole logs in Appendix 1.
- **3.5** Gas/water monitoring visits were undertaken on 17 and 24 August and 18 September 2018 and the results are presented in Appendix 6. Water monitoring data is also presented in Figure 1 and discussed in Section 3.17-3.19. Gas monitoring results are summarised in Table 7 and discussed in Section 5.8-5.13.
- **3.6** Upon completion of logging, sampling and in-situ testing, all boreholes were backfilled with compacted arisings and surface topsoil replaced.

Laboratory Testing - Geotechnical

- **3.7** The certified geotechnical laboratory test results are presented as Appendix 4.
- **3.8** A number of disturbed samples were taken for routine geotechnical classification testing, comprising moisture content and plasticity determinations, along with classification to the Unified Soil Classification Scheme (USCS) and NHBC Standards, plus acidity and sulphate analysis to BRE Special Digest 1 requirements. Results are tabulated below.



TABLE 1: INDEX TEST RESULTS AND CLASSIFICATION

BH No	Depth (m)	Sample of	Moisture Content (%)	Liquid Limit (%)	Plastic Limit (%)	Plasticity Index (%)	Plasticity / USCS	Consistency Index	<425um (%)	Modified Plasticity Index (%)	Volume Change Potential (NHBC)
WS1	2.0	CMF	26	62	23	39	СН	0.92	100	39	Med
WS1	3.5	CMF	24	63	22	41	СН	0.95	100	41	High
WS2	0.7	CMF	25	83	28	55	CV	1.05	100	55	High
WS2	1.0	CMF	26	63	22	41	СН	0.9	100	41	High
WS2	3.0	CMF	27	60	22	38	СН	0.87	100	38	Med
WS3	0.5	CMF	25	49	23	26	CI	0.92	100	26	Med
WS3	3.8	CMF	22	62	24	38	СН	1.11	100	38	Med
WS4	1.5	CMF	27	71	25	46	CV	0.96	100	46	High
WS4	2.5	CMF	25	61	24	37	СН	0.97	100	37	Med
WS5	0.5	CMF	20	50	22	28	CI/H	1.07	100	28	Med
WS5	1.7	CMF	22	61	23	38	СН	1.03	100	38	Med
WS6	0.5	CMF	21.7								
WS6	1.0	CMF	24.3								
WS6	1.5	CMF	24.7								
WS6	2.0	CMF	19.3								
WS6	2.5	CMF	18.8								
WS6	3.0	CMF	19.5								
WS7	1.5	CMF	25	59	24	35	СН	0.97	100	35	Med
WS7	2.5	CMF	20	57	22	35	СН	1.06	100	35	Med
WS8	0.5	CMF	20	44	22	22	CI	1.09	100	22	Med
WS8	2.0	CMF	22	57	21	36	СН	0.97	100	36	Med
WS9	1.3	CMF	23	58	23	45	СН	0.78	100	45	High
WS9	2.3	CMF	21	62	26	36	СН	1.14	100	36	Med
WS10	0.5	CMF	27	51	23	28	СН	0.86	100	28	Med
WS10	1.5	CMF	23	50	24	26	CI/H	1.04	100	26	Med
WS11	0.75	CMF	25	48	23	25	CI	0.92	100	25	Med
WS11	1.75	CMF	18	54	21	33	СН	1.09	100	33	Med

CMF = Charmouth Mudstone Formation



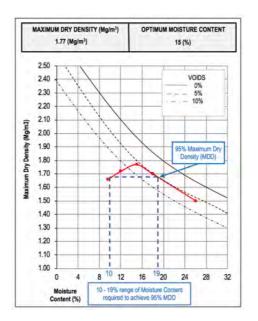
BH Ref	Depth (m)	Sample of	Total Sulphate SO4 (%)	Total Sulphur (%)	Total Potential Sulphate SO4	Oxidisable Sulphides SO ₄ (%)	pH Value in Soil	Water Soluble Sulphate (mg/l)	Accordi Special	Overall Classification According to BRE Special Digest 1 (2005)	
					(%)			SO4	DS	ACEC	
WS1	1.5	CMF	0.04	0.02	0.06	0.02	6.8	50	DS-1	AC-1	
WS1	2.5	CMF	0.19	0.07	0.21	0.02	7.9	840	DS-2	AC-2	
WS1	3.5	CMF	4.9	1.7	5.1	0.2	7.7	2280	DS-4	AC-4	
WS5	1.0	CMF	0.01	0.01	0.03	0.02	6.8	20	DS-1	AC-1	
WS5	2.0	CMF	0.03	0.01	0.03	<0.01	7.8	50	DS-1	AC-1	
WS5	3.0	CMF	0.03	0.02	0.06	0.03	7.5	70	DS-1	AC-1	
WS8	1.3	CMF	<0.01	<0.01	<0.03	<0.02	6.9	<10	DS-1	AC-1	
WS8	2.3	CMF	0.03	0.01	0.03	<0.01	7.8	20	DS-1	AC-1	
WS8	3.3	CMF	0.03	0.05	0.15	0.12	7.4	20	DS-1	AC-1	
WS9	0.7	CMF	0.04	0.02	0.06	0.02	6.0	<10	DS-1	AC-1	
WS9	1.7	CMF	0.01	<0.01	<0.03	<0.02	5.8	<10	DS-1	AC-1	
WS9	2.7	CMF	0.01	<0.01	<0.03	<0.02	7.4	<10	DS-1	AC-1	

TABLE 2: CHEMICAL TEST RESULTS AND CLASSIFICATION

CMF = Charmouth Mudstone Formation

3.9 A single representative sample of near surface cohesive material from WS3 was subject to a light hammer compaction test to determine the dry density/moisture content relationship, and the resulting compaction curve is shown in Figure 1 below.

FIG 1: MOISTURE CONTENT -v- DRY DENSITY (WS3/0.5-3.5m)





3.10 Given that suspected shear planes were locally encountered within the near surface weathered clay of the CMF, two disturbed samples were taken for a consolidated drained peak and residual shear box test to determine effective shear strength and effective cohesion soil parameters. The results are presented in Table 3 below.

TABLE 3: PEAK AND RESIDUAL ANGLE OF SHEARING RESISTANCE AND EFFECTIVE COHESION

Borehole No.	Depth	Sample of	Moisture Content (%)	Bulk Density (Mg/m³)	Dry Density (Mg/m³)	Peak Angle of Shearing Resistance (ǿ)	Peak Effective Cohesion (c')	Residual Angle of Shearing Resistance (ø'r)	Residual Effective Cohesion (c'r)
WS1	0.85m	CMF	19	1.46	1.23	18.5	6	12.0	3
WS8	0.8m	CMF	14	1.82	1.6	19.8	10	15.8	7

CMF = Charmouth Mudstone Formation

Laboratory Testing - Contamination

- **3.11** The contamination sampling scheme was conducted in accordance with BS10175:2011. Representative samples of topsoil and natural undisturbed soil were taken from the upper 0.6m of extracted ground. All samples were sent to UKAS accredited Concept Life Sciences laboratories in Manchester under chain of custody labelling where analysis selectively comprised the following:
 - Toxic and phytotoxic metals
 - pH
 - Soil organic matter content
 - Speciated polyaromatic hydrocarbons (PAH) (16 most common compounds)
 - Asbestos Identification
 - Organochlorine and organophosphorous insecticides
 - Topsoil BS3882: 2015
- **3.12** In the absence of groundwater during the short time the boreholes were left open during sitework, the potential risk to groundwater resources was instead determined by leachate analysis on five representative samples of topsoil, made ground and shallow natural material, tested to determine the leachable content of toxic and phytotoxic metals.



- **3.13** The certified contamination laboratory test results are presented as Appendix 2 and for convenience these have also been summarised to facilitate comparison against assessment criteria. All results and their implications upon the preliminary CSM are further discussed in Sections 8 and 9.
- 3.14 Three representative samples of topsoil were acquired for BS3882:2015 Topsoil analysis to determine suitability for retention within the proposed development as a multipurpose topsoil. Composite samples were taken from western fields (boreholes WS1-3), central fields (boreholes WS4, 8 and 10) and eastern fields (boreholes WS5-7, WS9 and WS11). The certified laboratory test results are contained within Appendix 2 but for ease of reference are also provided as certificates of analysis within Appendix 3. These results are further discussed in Section 5.15.

Discussion on Ground Conditions

3.15 Ground conditions appear to be commensurate with geological mapping. Beneath a thin mantle of topsoil and/or localised made ground all boreholes encountered undisturbed clay to termination, representing the recorded Charmouth Mudstone Formation. A summary of the observed strata is presented in Table 4 below.

Stratum **Base Depth** Notes (m) TOPSOIL: generally encountered as probable firm, dark brown, organic Encountered in 0.15 - 0.4 CLAY with many roots from overlying grass all boreholes except WS4 MADE GROUND: probable medium dense, sandy GRAVEL with many Encountered in borehole 0.4 roots. Gravel is brick and concrete WS4 only Encountered in WS1 and MADE GROUND: probable stiff, desiccated, light brown, slightly gravelly 0.35 - 0.5CLAY. Gravel is typically charcoal, brick and/or glass WS5 only CLAY: probable initially firm, mottled light brown and light grey desiccated CLAY. Possible relict shear surfaces identified between 0.65m and 0.85m depth in boreholes WS1-3 and WS5. Below 0.9-1.4m depth appearing Encountered to normally hydrated. With increasing depth becoming stiff, dark grey, with >4.45 terminal depth in all fossil and shell fragments, localised pockets of gypsum and showing relict boreholes mudstone structure. See specific logs for details (Charmouth Mudstone Formation) Depth to Water (m) Perched/Groundwater All boreholes dry

TABLE 4: SUMMARY OF OBSERVED STRATA



- **3.16** Based upon on-site visual and olfactory examination of the subsoil, and consistent with the site history there was nothing to suggest the presence of obviously significantly contaminated subsoil, however made ground was locally encountered, which appears to be restricted to the area proximal to existing buildings and access road.
- **3.17** The near surface soil was identified as entirely cohesive in composition and index testing on the CMF classifies this undisturbed material as inorganic clay of mostly high (locally intermediate or very high) plasticity and medium volume change potential (locally high) in accordance with NHBC Standards. Consistency index (CI) values were recorded between 0.86 and 1.14, with those values at >1.0 suggestive of mild desiccation, and the on-site visual assessment of undisturbed shallow subsoil would appear to confirm this. Given that the site is almost entirely grass and tree covered, the local flora would be expected to continue to desiccate the soil throughout the summer months with worst-case conditions expected at the end of the summer season, so depending upon the time of year of development actual conditions may vary from that reported.
- **3.18** All boreholes were dry during drilling, which in this Practice's experience is typical of the low-permeability CMF, however subsequent monitoring of those boreholes installed with standpipes (response zones of between 1.0m and 4.0m depth) indicated that groundwater does percolate slowly through the subsoil (most likely through fissures) and standing levels are shown in Figure 2 below.

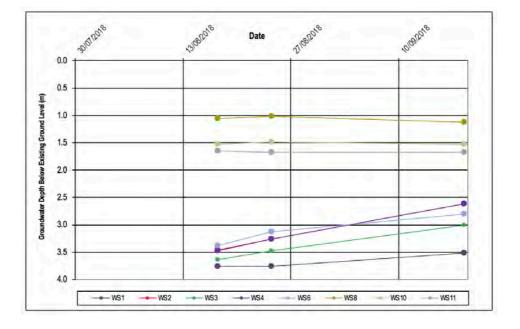


FIG 2: GROUNDWATER OBSERVATIONS



- **3.19** Our assessment of Figure 2 indicates that with the exception of WS2 the water level is shallower in those boreholes furthest upslope (WS8 and WS10-11), where levels were all initially recorded at fairly similar depths (1.05-1.65m) and remained constant during the monitoring period. The boreholes located further downslope (WS1, WS3-4 and WS6) including WS2 also initially recorded water at similar but greater depths (3.38-3.76m) and all expressed a similar characteristic gradual rise throughout the monitoring period.
- **3.20** The above would suggest that whilst in the short-term groundwater is unlikely to be encountered within newly excavated foundation or service trenches, the CMF does allow groundwater permeation, albeit at a slow rate due to the low permeability, therefore it is likely to be encountered within excavations (particularly deeper excavations) that are left open for any great period. As always, the groundwater level is of course subject to seasonal fluctuation according to prevailing weather conditions, and the situation encountered and described above could potentially change in the future, especially in a period of seemingly ever-apparent but unpredictable climate change.

Percolation Testing - Soakaway Feasibility

3.21 Two falling head percolation tests were undertaken separately within boreholes WS1 and WS6 into the undisturbed Charmouth Mudstone Formation, and summary results are shown below in Table 5. Due to negligible recorded drainage/outflow it has not been possible to calculate soil infiltration rates or undertake repeat tests within either of the two test locations.

Borehole No.	Test Zone Depth (m)	Approximate Soil Infiltration Rate (m/sec)	Approximate time to drain to 50% storage (hours)
WS1	0.34-4.45	N/A	>24
WS6	0.24-4.45	N/A	>24

TABLE 5: SUMMARY OF PERCOLATION TEST RESULT

3.22 BRE guidance states that soakaways should be feasible where infiltration rates indicate that water would drain to 50% effective storage capacity within a period of 24 hours. Due to insufficient infiltration this was not achieved within any of the test holes



and the results in Table 5 are considered to be representative of the entire site. The foregoing suggests that the site is not suitable for adoption of a soakaway (SUDS) drainage system and it is therefore recommended that alternative drainage options are sought. It is anticipated that surface-water attenuation pond(s) may already be the favoured option.

4 <u>GEOTECHNICAL DESIGN REPORT</u>

4.1 The site investigation works achieved by the eleven boreholes have proven ground conditions beneath the site to be in accordance with both recorded mapping and previous comparable experience. Beneath a thin surface mantle of topsoil and/or made ground all boreholes encountered undisturbed clay representing a normal weathering profile of the recorded Charmouth Mudstone Formation, which appeared locally affected by landslip.

Slope Stability

- 4.2 As previously identified during the Phase 1 researches, geological mapping records a swathe of landslipped ground that extends around the western and northern sides of Battledown hill and the conjectured easternmost edge of which extends across the western half of the site. Whilst landslipping is likely to have occurred in geological history our walkover survey revealed no obvious tell-tale signs of historic/ongoing instability (i.e. back scars or hummocky ground) although it is recognised that this assessment was hampered by long grasses growing at surface.
- **4.3** Subsequent intrusive investigation has identified possible relict shear surfaces at shallow depth only (between 0.65m and 0.85m depth) in boreholes WS1-3 and also WS5, however in all cases the condition of the shear surface was poorly defined.
- **4.4** Given the gradient of the existing slope it is anticipated that any development proposal will likely require cuts to be made into the slope. The presence of a 'suspected shear surface' suggests that care needs to be taken that any such interfaces are not exposed in bulk excavation as this could leave the overlying mass effectively unsupported. Given that the suspected shear surface was identified between 0.65m and 0.85m depth, this would indicate that this scenario is possible. Given the spacing of the boreholes during the current investigation it may be prudent to undertake



supplementary investigation (once a proposed layout is made available) to clarify those plots potentially affected. Again subject to the proposed development layout, a detailed slope stability assessment may be necessary and this Practice can provide further assistance if required.

- **4.5** Given the shallow depth of the suspected shear surface, foundation deepening beyond NHBC required depths (as discussed below) will not be necessary, although it may be prudent to reinforce the foundations of those potentially affected plots as a precaution, and upslope walls may need to be designed as retaining structures if they support the upslope ground.
- **4.6** It is recommended that retaining wall design be based upon residual shear strength values for the clay (suitably factored as per Eurocode guidance) of $C'_r=2 \text{ kN/m}^2$ and $\emptyset'_r=9.5^\circ$. Please note that water monitoring recorded sub-artesian conditions with the water level locally rising to 1.02m (WS8) below existing ground level so care will need to be taken during excavations.

Foundation Design

- **4.7** The natural weathered cohesive soils of the CMF classify as of mostly high plasticity and medium volume change potential, however it is recognised that almost 25% of the samples tested recorded as high volume change potential. Given both the lateral and vertical spread of 'high' test results together with the spacing of borehole locations, as a precaution we have provisionally adopted a site-wide high volume change potential for the site, which (following NHBC Standards) means that a minimum founding depth of 1.0m is required, or greater within the radius of influence of trees and obviously subject to those foundations also penetrating through any localised softer, infilled or disturbed deposits to found in competent undisturbed and normally hydrated natural material, below any observed shear planes.
- **4.8** Consideration has been given as to whether any foundation deepening is required (beyond the above minimum) to account for potential tree root activity. Site observations indicate that there are significant numbers of semi-mature and mature trees along field boundaries, including amongst others hawthorn and oak (of high water demand) and beech and ash (of moderate water demand). Given the high number of trees present it is recommended that a detailed tree identification survey is undertaken; once complete plot-specific foundation depths can be calculated for those plots



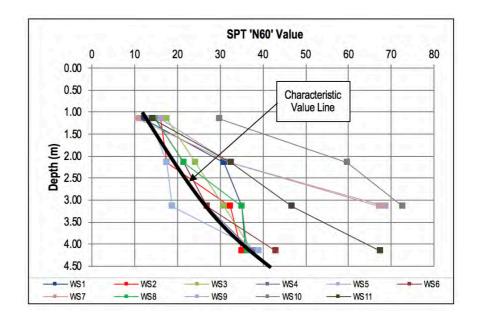
Job No. 4360/2 Page No. 12

affected by future root growth and possible existing desiccation, however it is understood that a final proposed development layout is not yet available.

- **4.9** Those buildings within the zone of influence of trees will require heave protection in the form of a 70mm thick compressible membrane against the inside face of all external foundations deeper than 1.5m in order to overcome potential unbalanced lateral heave forces (unless NHBC is satisfied that the soil is not desiccated). Such protection should be applied on the inner face of external foundation walls only, with the lower 0.5m left unprotected. The same buildings will also require suspended ground floor slabs, which should incorporate a subfloor void of 150mm for insitu concrete or 300mm for pre-cast concrete and timber floors.
- **4.10** Design calculations in Eurocode 7 (BS EN 1997-1) require the establishment of design values for actions, ground properties and ground resistances, definition of the limits that must not be exceeded (usually a serviceability limit state), the setting up of calculation models for the relevant ultimate or serviceability limit state, and showing by such calculation that these limits will not be exceeded. Design values for such calculations are derived by applying partial factors to characteristic values for actions, ground properties and ground resistances, and based upon the foregoing geotechnical model and following the requirements of Design Approach 1, both Combination 1 and Combination 2 calculations have been undertaken. This Practice has adopted the Combination 2 calculation for foundation design as this applies partial factors to resistances rather than actions and therefore provides a slightly more conservative value. Calculation sheets can be presented upon request.
- 4.11 BS EN 1997-2:2007 and BS EN ISO 22475-1:2006 require quality class 1 samples for determination of soil shear strength, and such samples can only be obtained by category A sampling methods. To avoid the costly complexities of such sampling insitu tests can alternatively be undertaken, the borehole standard penetration test (SPT) being the most commonly adopted method. Field results are adjusted or 'normalised' in accordance with Eurocode requirements (BS EN ISO 22476-9:2009), to enable the generation of characteristic values of undrained shear strength that can then be used for determination of bearing resistance as described above.
- 4.12 Uncorrected SPT N-values are shown on the borehole logs and normalised N-values shown are also presented as N₆₀ versus depth in Figure 3. Equivalent undrained shear strength has subsequently been calculated which also takes account of plasticity index values.







4.13 Using a characteristic SPT N₆₀ value of 12 at 1.0m depth, based on a conventional two-storey residential line load of 45kN/m, the design bearing resistance (bearing capacity) for a standard 0.6m wide strip foundation is estimated to be approximately 118kN/m², which exceeds the likely bearing pressure and confirms suitability. Similar calculations demonstrate only marginal suitability for 0.45m wide foundations at this depth (bearing capacity of 88kN/m²), indeed this continues with greater depth. Design bearing resistance is plotted against depth in Figure 4 below, so that values can be assigned to any other depths as necessary due to tree influence.

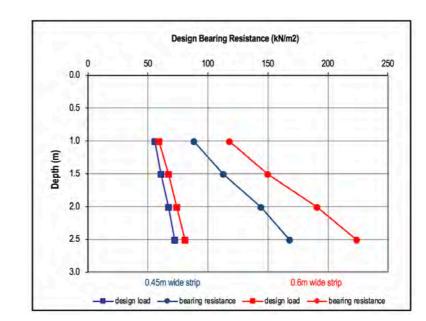


FIG 4: DESIGN BEARING RESISTANCE -v- DEPTH



- **4.14** The results of acidity and sulphate testing presented in Table 2 show that buried concrete associated with foundations and floor slabs constructed up to 2.3m depth can be designed to Design Sulphate Class DS-1 and Aggressive Chemical Environment for Concrete Class ACEC-1 in accordance with BRE Special Digest 1 (2005), i.e. no special measures required. For foundations in excess of 2.3m depth it is recommended that the concrete grade be increased to DS-2, AC-2 and in the unlikely event that foundation trenches will be excavated to 3.5m depth then it is recommended that the concrete grade be increased again to DS-4, AC-4. Similar requirements apply to concrete drainage pipes.
- **4.15** Shallow excavations should remain stable and as previously discussed in Section 3.19 in the short term it is not anticipated that groundwater will be encountered. As always it is recommended that any excavations are not left open and unsupported for any longer than necessary, and if water is encountered, in order to avoid potential softening of the founding horizon it should not be permitted to sit on the foundation base. As always groundwater levels may vary seasonally, and water may therefore be encountered at levels in variance to those recorded by this investigation.

Pavement Design

4.16 With regard to pavement design for external hardstand, near surface plasticity index values of between 22% and 28% within the near surface cohesive clay suggests a California Bearing Ratio (CBR) of approximately 3-4% at 0.5m depth. As always it is recommended that insitu testing be carried out closer to the time of construction to obtain a more accurate bearing ratio. The clay soil is not considered to be frost-susceptible, however the Local Authority should be able to advise based upon their previous experience in the area.

Material Suitability In Earthworks

4.17 Should the development proposal include surface run-off attenuation or "balancing" ponds, the following gives outline recommendations on material suitability for incorporation into earthworks. As shown in Figure 1 a light hammer compaction test on a sample of clay from WS3 at 0.5-3.5m depth indicates that a maximum dry density of 1.77 Mg/m³ can be achieved at an optimum moisture content (OMC) of 15%. On the assumption that excavated materials would be recompacted to 95% of the maximum dry density (MDD), the compaction curve gives a moisture content range of



between 10% and 19% to achieve 95% MDD or greater. Review of moisture content test results in Table 1 indicates that arisings will require interim drying within any earthworks in order to achieve the 95% criterion, although if the required density were reduced below 95% MDD then more of the material would become potentially suitable direct from cut to fill. This situation will vary seasonally and also excludes the effects of stockpiling of materials before use.

Recommendations for Monitoring of Ground Conditions During Construction

- **4.18** In view of the importance of founding on natural ground, a careful watch must be maintained during all foundation excavations to ensure that this requirement has been satisfied.
- **4.19** Consideration should be given to access into/around the site since the surface soils have the potential to be subject to softening during periods of sustained wet weather.
- **4.20** Due to the potential for cohesive soils to shrink and swell, inspection during foundation excavations should ensure that no live roots or evidence of desiccation is visible at the founding horizon.
- **4.21** In the event of any doubt in the above matters, this Practice would be pleased to attend site as instructed.

5 <u>CONTAMINATION RISK ASSESSMENT, TOPSOIL SUITABILITY AND SOIL</u> <u>WASTE CLASSIFICATION</u>

Human Health

5.1 The contamination risk assessment has been carried out in general accordance with the methodology described within Appendix 1. Testing has included samples of the near-surface topsoil and undisturbed clay to assess their suitability for retention within the development proposal. In view of the nature of the proposals Tier 1 risk modelling has adopted the '*residential*' land use scenario, including the pathway of direct ingestion via vegetables grown for consumption, and the 'critical receptor' is taken as a female child of age class 1-6.



5.2 Laboratory test results are presented in Appendix 3 and have also been summarised in Table 6 below.

Determinand	Maximum Measured Concentration (mg/kg)	LQM/CIEH S4UL Residential with plant uptake (mg/kg) \$	Tests Undertaken (No.)	Exceedances (No.)	Notes
Arsenic	38	37	22	1	WS10/0.2m
Cadmium	1	11	22	0	
Chromium*	66	910	22	0	
Lead	190	200**	22	0	
Mercury	<1	40	22	0	
Selenium	<3	250	22	0	
Nickel	46	180	22	0	
Copper	77	2400	22	0	
Zinc	190	3700	22	0	
Asbestos Fibres	CHR	N/A	1	1	WS4/0.25m
PAH compounds	Various	Various	5	0	
Insecticides	All below LOD	Various	3	0	
Notes:					
* assumed all chrom	ium on site is in trivale	ent form			
** former C4SL used	in absence of S4UL				
\$ based on soil orga	nic matter = 2.5%				

TABLE 6: COMPARISON OF SOIL CHEMICAL TEST RESULTS WITH GUIDELINE VALUES

- **5.3** The findings presented in Table 6 indicate that there are no elevations of phytotoxic metals, PAH or insecticide compounds above Tier 1 Generic Assessment Criteria (GAC). It is however noted that loose fibre(s) of ACM were locally identified (Chrysotile) along with a single elevation of the toxic metal arsenic that may pose a risk to the health of future site users and these have been considered in more detail below.
- 5.4 Firstly considering arsenic, a value of 38mg/kg (WS10/0.2m) was recorded within near surface natural clay which very mildly exceeds the GAC-S4UL of 37mg/kg. Progression has therefore been made to a Tier 2 site-specific assessment which includes statistical analysis using the CIEH Statistical Calculator and assessment using site-specific parameters within CLEA v1.071. The CLEA software has calculated a site-specific assessment criteria (SSAC) value of 36.5mg/kg. All results came from non-targeted investigation so are therefore deemed permissible for



inclusion within statistical analysis, and using such data an Upper Confidence Limit (UCL) of 22.6mg/kg has been determined which does not exceed the SSAC. The isolated elevated value of arsenic is therefore not considered to pose a significant risk to the health of future site users.

- 5.5 Suspected ACM was identified during the walkover survey being used as corrugated roof sheeting on derelict farm buildings and laboratory testing has identified loose fibre(s) of Chrysotile within a single sample of surface made ground (WS4/0.25m) in the farm yard. it may be prudent to commission a specialist to undertake a formal asbestos survey prior to any demolition.
- 5.6 It is current recommended practice to remove all asbestos from residential developments, not only for the protection of future site users but also to protect groundworkers, and all such material will need to be disposed of off-site at a suitably licensed landfill. It is recommended that some further investigation is undertaken once all existing buildings have been demolished to delineate the area surrounding not only WS4 but also the wider farm yard that may be affected, determine the volume of made ground requiring off-site disposal and also clarify whether the subsequent waste stream classifies as hazardous. Note that if only isolated fragments are found rather than free fibres within the soil, then a simplified 'manual pick' strategy may be sufficient to remove the risk. Please note that the submission of a formal remedial strategy may be requested by the relevant authority detailing the method and timescales of such works. Immediately following the remedial works, it will be necessary to undertake validation sampling on the exposed formation to ensure that all contaminated material has been adequately removed with a final verification report produced, again to satisfy the relevant authority. Replacement soil will need to be uncontaminated and suitable for a residential development and ideally come with pre-certification confirming its suitability. This Practice can provide further assistance with the foregoing if required.

Water Supply Pipework

5.7 In addition to the above, consideration has been given to the potential effects of recorded concentrations on new water utility pipework. Given the general absence of made ground and negligible risk from organic contaminants there ought to be no requirement for upgraded barrier pipework and the results of the contamination testing undertaken as part of this investigation would seem to support this. As always it is recommended that advice be sought from the local regulatory authority prior to ordering, since it is possible that their specific in-house thresholds may differ markedly



from those within the most recent guidance by UK Water Industry Research (UKWIR) report "Guidance for the Selection of Water Supply Pipes to be used in Brownfield Sites" (2010).

Landfill Gas and Radon Gas

- **5.8** It was previously established during desk study researches that the site is located within proximity to a single recorded historical landfill site located 180m to the north, as well as a backfilled reservoir to the east and former clay pits to the west, and may therefore be affected by landfill gases migrating from one or more of these sources.
- **5.9** The landfill gas risk assessment has been undertaken in general accordance with BS8485:2015 "Code of practice for the design of protective measures for methane and carbon dioxide ground gases for new buildings", and with reference to Construction Industry Research and Information Association (CIRIA) 665 'Assessing risks posed by hazardous ground gases to buildings' (2007).
- **5.10** As shown in Appendix 7 the recent monitoring has recorded maximum concentrations of methane and carbon dioxide of 0% and 5.3% respectively, with a maximum steady state flow rate of +0.2 l/hr. Worst case low (and falling) atmospheric pressure was recorded during one out of the three monitoring visits.
- **5.11** On this basis the implied maximum Characteristic Situation (CS) is derived by consideration of the maximum hazardous gas flow rate calculated from each monitoring well during the recent monitoring rounds, as shown in Table 7 below.

BH Ref	Maximum Steady State Flow (I/hr)	Maximum Peak Gas Concentrations (%) Methane Carbon Dioxide		Concentrations (%) Gas Flow Rate (I/hr) Characteristic		Worst-Case Hazardous Gas Flow Rate (l/hr) Q _{hg}		Worst-Case Characteristic Situation			
				$Q_{hg}CH_4$	Q _{hg} CO ₂	CH₄	CO₂	CH₄	CO₂	CH₄	CO₂
WS1	+0.2	0.0	1.7	0.0	0.0034	1	1				
WS2	0.0	0.0	0.6	0.0	0.006	1	1				
WS4	+0.1	0.0	5.3	0.0	0.0053	1	1	0.0	0.011	1	1
WS6	+0.1	0.0	1.5	0.0	0.0015	1	1				
WS11	+0.1	0.0	1.4	0.0	0.0014	1	1				

TABLE 7: SUMMARY GAS MONITORING RESULTS AND MAXIMUM CHARACTERISTIC SITUATION



NOTES:	
Qhg	= equivalent to GSV in C665
	Implied Characteristic Situation based on individual borehole data
	Worst-case gas flow rate and Characteristic Situation based on maximum observed flow rate and concentrations from any borehole

- **5.12** As shown in Table 7 above, based on both peak and worst-case monitoring results the overall site classification is 'CS1' indicating a very low hazard potential. It is recognised however that a value of 5.3% was recorded for Carbon Dioxide, which exceeds the "typical maximum" of 5% and further consideration has therefore been given as to whether an increase to CS2 classification may be appropriate. Given the only nominal exceedance of the typical maximum and that subsequent monitoring rounds (during worst-case low and falling atmospheric pressure) did not record any further exceedances the original site classification of CS1 is still considered appropriate. Landfill gas protection measures are not therefore considered necessary within new development.
- **5.13** Consultation of the BRE Report BR211 "Radon: guidance on protective measures for new buildings" (2015) suggests that no radon gas protection measures are required in new development at this site.

Controlled Waters

5.14 In the absence of groundwater within the boreholes at the time of the intrusive works, the risk to controlled waters has instead been assessed by leachate analysis on five representative soil samples of topsoil, made ground and shallow natural material, each tested to determine the leachable content of toxic and phytotoxic metals. It will be seen within Appendix 2 that there are no recorded elevations above respective Water Framework Directive (WFD) thresholds for groundwater. In view of the foregoing no additional pre-construction remedial measures in respect of controlled waters are considered necessary.

Topsoil Suitability for Retention

5.15 Three composite samples (Western, Central and Eastern Fields) have each been tested in accordance with BS3882:2015 "*Specification for Topsoil*" to determine the suitability of the existing topsoil for retention within the proposed development. As shown in Appendix 3 the Certificates of Analysis classify all three composite samples



as 'silty clay' due to relative sand, silt and clay contents, which unfortunately means that all three samples fall outside the acceptable limits for a multi-purpose topsoil. In addition to the foregoing, the Western Field sample was also noted to have an excessive organic matter content, and both Central and Eastern Field samples had nutrient deficiencies. It may be possible to recover the topsoil to multi-purpose quality and it is recommended that advice be taken from a landscaping/topsoil specialist.

Waste Classification for Off-Site Disposal of Arisings

- 5.16 In accordance with current legislation all soil arisings generated for disposal as part of this development site are by definition a "commercial waste" and will be classified as both a directive and a controlled waste. Should it be necessary to remove from site any surplus excavation arisings then as per the European Waste Catalogue (EWC) these will be coded 1705, that is "soil (including excavated soil from contaminated sites), stones and dredging spoil".
- 5.17 Using the HazWasteOnline software and in accordance with Technical Guidance Waste Management 3 (TGWM3) 1st Edition, 2015) the contamination test results obtained for that material have been compared with respective threshold data as set out in TGWM3 in order that this specific waste stream can be classified. As shown in Appendix 6, this material would be classified as a "Non-hazardous Mirror Entry" under EWC Code 170504 (soil and stones that do not contain the tested dangerous substances above the respective threshold value). Such materials can therefore be disposed of at a suitably licensed "non-hazardous" landfill site, which will require the contamination test data undertaken as part of this investigation.
- 5.18 The presence of chrysotile fibres within localised near surface made ground means that this specific waste stream would currently be classified as a 'Hazardous Mirror Entry' under EWC Code 170503* (soil and stone containing dangerous substances). Unless and until an asbestos quantification test proves a fibre content of <0.1% such material will require disposal at a suitably licensed 'hazardous' landfill site.</p>
- 5.19 On the assumption that all other non-hazardous arisings are being considered for disposal as inert waste to take advantage of a lower tipping rate, Waste Acceptance Criteria (WAC) testing has been undertaken on three composite samples (one each from Western, Central and Eastern Fields), mostly comprising natural CMF but where appropriate also containing made ground (Central Fields samples only). As shown in Appendix 5, all tested determinands from both the Central and Eastern composite



samples fall within acceptable thresholds for inert waste (EWC code 17-05-04). Considering the Western Fields composite sample, it should be noted that this sample recorded both an elevated 'sulphate' value of 6900mg/kg, which exceeds the threshold of 1000mg/kg and an elevated 'total dissolved solids' value of 8100mg/kg, which exceeds the threshold of 4000mg/kg. The foregoing therefore suggests that the arisings from the Western Fields will not qualify as inert waste. It is recommended that the attached WAC results (Appendix 5) and contamination test data (Appendix 2) are provided to the chosen landfill operator for their own assessment of acceptability in advance of soil arrival.

Caveats

- **5.20** In line with best industry practice the scope of contamination testing has been based upon the site history, current land usage and actual findings, with reference where necessary to DoE Industry Profiles and DEFRA/EA guidance. To the best of our knowledge information concerning the land quality assessment is accurate at the date of issue, however subsurface conditions including ground contamination may vary spatially and with time. There may be conditions pertaining to the site not disclosed by the above sources of information, which might have a bearing upon the recommendations made, were such conditions known. We have however used our professional judgement in order to limit this during the investigation.
- 5.21 The conclusions and recommendations made in respect of land quality do not address any potential risks to site operatives or ground workers during the construction stage. These issues should be addressed by the Principal Contractor in accordance with the relevant statutory procedures and regulations (CDM Regulations 2015).
- **5.22** It is important that these limitations be clearly recognised when the findings and recommendations of this report are being interpreted. Additional assessment may be necessary should a significant delay occur between report date and implementation of the proposed scheme to which it relates.



6 <u>REFINED CONCEPTUAL SITE MODEL</u>

6.1 In view of the above discussions the preliminary conceptual site model has been refined as shown in Figure 5 and Table 8 below.

FIG 5: REFINED CONCEPTUAL SITE MODEL (NTS)

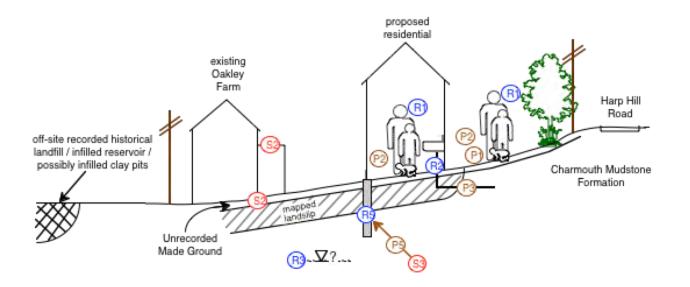


TABLE 8: SUMMARY OF POTENTIAL / IDENTIFIED POLLUTANT LINKAGES

Potential	-			Rece	ptors				Refined	
Sources	Pathways	R1	R2	R3	R4	R5	R6	Comments	Risk Rating	Remedial/Mitigation Requirements
ON-SITE										
	P1									
	P2	х					х			Further investigation recommended
	P3									following building demolition to delineate affected area requiring
S2	P4			4		4		Chrysotile asbestos recorded in near surface made ground near	High	excavation and off-site disposal, or simple manual pick to remove ACM
	P5							Oakley Farm buildings		fragments. Supplementary quantification testing recommended to
	P6									help classify waste
	P7									
	P1									
	P2									
	P3									Concrete classification of DS-1/AC-1 suitable for foundations and floor slabs
S 3	P4							Elevated sulphate/sulphide recorded within Charmouth	High	up to 2.3m depth. Below 2.3m depth increase to
	P5					Х		Mudstone Formation		DS-2/AC-2 required. Below 3.5m depth increase to
	P6									DS-4/AC-4 required.
	P7									
OFF-SITE										
SOURCES	S 2	Chrysotile	Asbestos i	dentified wit	nin near sur	face made (ground (with	nin vicinity of farm buildings)		
SUURCES	S 3	Natural C	harmouth M	udstone For	mation					
	P1	Direct der	mal contact	or ingestion	via soil atta	ached to veg	getables			
	P2	Inhalation	of dust & va	apours						
	P3	Permeatio	on into new	water supply	v pipework					
PATHWAYS	P4	Vertical le	aching in ur	nsaturated z	one and late	eral migratio	n in saturat	ted zone		
	P5	Direct cor	ntact with hig	gh sulphate-	bearing clay	y				
	P6	Landfill ga	as migration	through uns	aturated zo	one and acci	umulation w	vithin confined spaces		
	P 7	Radon ga	s migration	through uns	aturated zo	ne and accu	imulation w	ithin confined spaces		
	R1									
	R2									
RECEPTORS	R3	Groundwa	ater (CMF is	a Seconda	y Undiffere	ntiated aqui	fer)			
NEVER I UNS	R4	Surface w	raters							
	R5	Concrete	Foundation	S						
	R6	6 Adjacent site users (residential)								



7 CONCLUSIONS AND RECOMMENDATIONS

- 7.1 The foregoing discussions and recommendations are based upon the results of an intrusive ground investigation comprising boreholes plus insitu testing and laboratory geotechnical and contamination testing. The boreholes appear to present a consistent pattern of subsoil conditions concordant with recorded geological mapping comprising undisturbed Charmouth Mudstone Formation below a thin surface mantle of topsoil, localised made ground and localised near surface suspected landslip affected strata. As always however a careful watch should be maintained for any anomalous conditions during site stripping and excavation, which should be reported back to this Practice for further investigation and assessment. Some supplementary ground investigation and assessment should be undertaken as the site is broken down into smaller development parcels.
- **7.2** The intrusive investigation has proven topsoil/made ground up to 0.5m depth, which directly overlies the recorded undisturbed cohesive CMF, proven to terminal depth in all boreholes. The CMF was mostly recovered as probable initially firm, mottled light brown and light grey desiccated CLAY, appearing normally hydrated below 0.9-1.4m depth. With increasing depth becoming stiff, dark grey, with fossil and shell fragments, localised pockets of gypsum and showing relict mudstone structure.
- **7.3** Possible relict shear surfaces were identified between 0.65m and 0.85m depth in boreholes WS1-3 and WS5. All boreholes remained dry and stable during the time left open while drilling, however subsequent piezometer readings recorded subartesian standing water at depths of as shallow as 1.02m from surface. The short-term stability of side walls within open excavations for foundations and services is unlikely to be an issue during construction, however some care will obviously need to be taken within those plots falling within the area affected by landslip as exposing the shallow shear plane in bulk excavation could potential lead to an unsupported slope. Dependent on the proposed development layout it is likely that some slope retention may locally be necessary and it is recommended that retaining wall design be based upon factored residual shear strength values of $C'_r=2 \text{ kN/m}^2$ and $\mathcal{O}'_r=9.5^\circ$.
- **7.4** Foundations will need to penetrate any near surface disturbed, softer or desiccated ground to found within normally hydrated soil of the undisturbed CMF at a minimum depth of 1.0m, with foundation deepening and suspended ground floor slabs likely for any buildings located within the zone of influence of trees. Heave protection will only be necessary if desiccation is present within soil beneath building footprints at the time



of construction. At the minimum depth founding horizon the design bearing resistance has been calculated as being suitable for a typical two storey dwelling on 0.6m wide foundations. Narrower 0.45m wide foundations are only marginally suitable so should not be considered without a more detailed assessment.

- 7.5 Buried concrete in open excavations for conventional strip/trenchfill foundations and floor slabs up to 2.3m depth can be designed to concrete classification DS-1/AC-1. i.e. no special precautions required. Should foundations or concrete drainage infrastructure be required to exceed 2.3m depth then the concrete classification will need to be increased to DS-2/AC2 and for foundations in excess of 3.5m depth this increases again to DS4/AC/4. Deep excavation arisings from >2.3m depth should not be placed as backfill against concrete that is <DS/AC2 classification (or DS/AC4 if from > 3.5m depth)
- **7.6** In terms of proposed external pavement design a CBR value of 3-4% is considered appropriate (based on correlation from index test results only) and such material is unlikely to be frost susceptible. As always we recommend that in-situ tests be undertaken closer to the time of construction once proposed road layouts are known.
- **7.7** The soils found beneath the entire site are of inadequate permeability to be suitable for a soakaway (SUDS) drainage system, therefore an alternative method of surface-water removal will be required.
- **7.8** Contamination risk assessment has shown that the site is mostly uncontaminated in terms of risk to both human health and controlled waters, however Chrysotile asbestos was locally recorded within near surface made ground in proximity to the existing farm yard buildings and further works are recommended following demolition to delineate the affected area and to quantify the waste stream.
- **7.9** BS3882:2015 Topsoil testing has suggested that the existing topsoil across the entire site is currently unsuitable for reuse as a multi-purpose topsoil within a residential end-use primarily due to a Silty Clay textural class falling outside the required acceptable limits. Additionally, the topsoil was also found to be deficient in nutrients. It is recommended that a landscaping/topsoil specialist be consulted to determine whether the topsoil can be recovered/improved to confirm with BS3882:2015 requirements.
- **7.10** With regard to the off-site disposal of arisings, the majority of soil classifies as a 'Non-Hazardous Mirror Entry' and therefore can be disposed of at a suitably licensed non-



hazardous landfill site, however the localised near surface made ground containing asbestos fibres currently classifies as a 'Hazardous Mirror Entry' and in the absence of an asbestos quantification test (which might downgrade it to non-hazardous) this material will require disposal at a hazardous landfill site. WAC testing has identified that arisings from Central and Eastern Fields also classify as inert waste, although arisings from Western Fields classify as non-hazardous (stable non-reactive) waste due to exceedances of both sulphate and total dissolved solids.

- **7.11** There is no requirement for landfill gas protection measures and in line with BGS and HPA records no radon protection measures are necessary within new construction at this site.
- **7.12** Should planning consent be subject to certain conditions, this report and attachments should be lodged with the local planning authority, such that they can update their records.
- **7.13** The above recommendations must not be used in respect of any development differing in any way from the proposals described in this report, without reference back to this Practice or to another geotechnical/geo-environmental specialist. This report is subject to our standard terms and conditions.

8 <u>REFERENCES</u>

Geotechnical
BS EN 1997-1:2004 'Geotechnical Design - General Rules'
BS EN 1997-2:2007 'Geotechnical Design - Ground Investigation and Testing'
British Standards Institute, BS5930:2015 'Code of Practice for Ground Investigations'
National House Building Council (NHBC) Standards: Chapter 4.2 'Building Near Trees' (2016)
BS EN 14688: 'Geotechnical Investigation and Testing - Identification and Classification of Soil Part 1 Identification and Description' (2002)
BS EN 14688: 'Geotechnical Investigation and Testing - Identification and Classification of Soil Part 2 Principles for a Classification' (2004)
BS EN 14689: 'Geotechnical Investigation and Testing - Identification and Classification of Rock Part 1 Identification and Description' (2003)
British Standards Institute, BS 1377: 'British Standard Methods of Test for Soils for Civil Engineering Purposes', Parts 1 - 9, (1990)
Highways Agency Interim Advice Note 73/06 Rev.1 (2009) Design Guidance for Road Pavement Foundations
Building Research Establishment (BRE) Special Digest 1 'Concrete in Aggressive Ground' (2005)
British Geological Survey (England & Wales) Sheet SO 92 SE and 'online'
Building Research Establishment (BRE) Digest 365 "Soakaway Design" (2016)
Department of Transport Series 600: 'Specification for Earthworks' (1991)
Environmental

British Standards Institute, BS 10175: 'Code of Practice for the Investigation of Potentially Contaminated Sites' (2011)



Environment Agency CLR 11: 'Model Procedures for the Management of Land Contamination'

Environment Agency/National House Building Council (NHBC) R&D 66 'Guidance for the Safe Development of Housing on Land Affected by Contamination' (2000)

Chartered Institute of Environmental Health (CIEH)/Land Quality Management Limited (LQM). The LQM/CIEH 'Generic Assessment Criteria for Human Health Risk Assessment' (2nd Edition). Land Quality Press

DEFRA: SP1010: Development of Category 4 Screening Levels for Assessment of Land Affected by Contamination - Policy Companion Document (2014)

CIEH/LQM. 'S4ULs for Human Health Risk Assessment' (2015); Land Quality Press"

Department of the Environment, Transport & the Regions: 'The Environmental Protection Act 1990: Part IIA' (2000)

Construction Industry Research & Information Association (CIRIA) 665: 'Assessing Risks Posed by Hazardous Ground Gases to Buildings' (2007)

CIRIA C735:2014 'Good Practice on the Testing and Verification of Protection Systems for Buildings Against Hazardous Ground Gases'

British Standards Institute, BS8485: 'Code of practice for the design of protective measures for methane and carbon dioxide ground gases for new buildings' (2015)

Building Research Establishment (BRE BR211): Radon - 'Guidance on protective measures for new buildings' (2015)

Environment Agency. 'River Basins Typology, Standards and Groundwater (Water Framework Directive) (England and Wales) Directions' (2010)

Environment Agency. 'The Water Framework Directive (Standards and Classification) Directions (England and Wales)' (2015)

The Water Supply (Water Quality) Regulations 2000 (Amendment) Regulations (2007)

UK Water Industry Research Limited (UKWIR). 'Guidance for the Selection of Water Supply Pipes to be used in Brownfield Sites' (2010)

Technical Guidance Waste Management 2 (TGWM2, EA Version 3.0, May 2013)

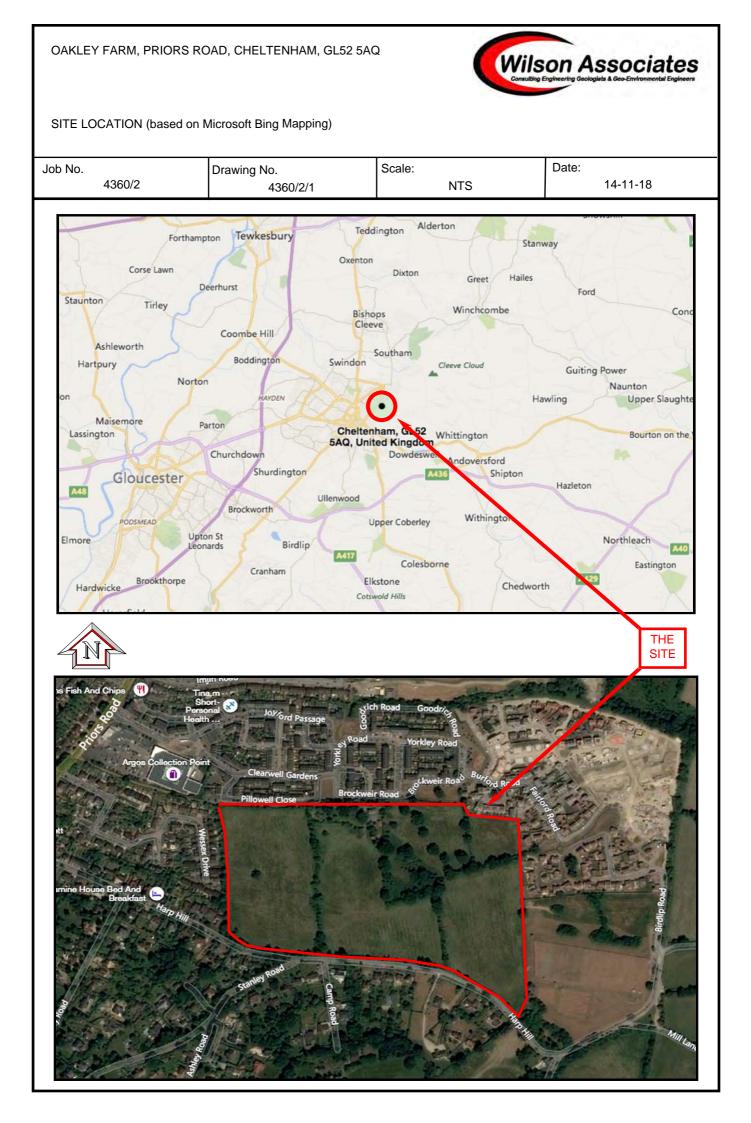
Building Research Establishment (BRE)- 'Cover Systems for Land Regeneration' (2004)

Environment Agency (www.environment-agency.gov.uk)

Zetica (www.zetica.com)

Google Earth (current and historical aerial mapping plus street view)

Wilson Associates (Consulting) Limited report ref 4360, dated June 2018







Job No. 4360/2

APPENDIX 1

BOREHOLE LOGS (INCLUDING PHOTOGRAPHS)

Wilson Associates

Consulting Engineering Geologists & Geo-Environmental Engineers

KEY TO BOREHOLE LOG SYMBOLS

Symbol	Explanation
D or J	Small Disturbed Sample (tub or jar sample)
В	Large Disturbed Sample
U	Undisturbed Sample
W	Water Sample
U70	Undisturbed Sample

Undrained Shear Strength Test (HSV)

90	Hand vane - direct reading in kN/m ²
Standard Pe	netration Test (SPT)
15	SPT 'N' Value (BS EN ISO 22476-3:2005)
125/50	Where full test drive not completed, penetration (125mm) and blow count (50) recorded
NR	No effective penetration
Water	
1	Water struck
1 ⊻	Water standing

Test/Core Range

TCR	Total Core Recovery - as percentage of core run. Where value significantly exceeds 100%, a note is given on remarks on log
SCR	Solid Core Recovery - as percentage of core run. Note: assessment of solid core is based on full diameter
RQD	Rock Quality Designation - the amount of solid core greater than 100mm expressed as percentage of core run
	Where SPT has been carried out at beginning of core run, disturbed section of core excluded from SCR and RQD assessment

Instrumentation

Ē		
Ē		
E		

Bentonite Seal

Solid / Perforated Standpipe

Granular Response Zone



BOREHOLE LOG

Project							BOREHOLE No									
Oakley Farm, Priors Road, Cheltenham GL52 5AQ												\ <i>٨/</i>	61			
Job No							Level (c.m, AOD) Co-Ordinates (c.)					VV.	VS1			
43	360/2		3	0-07-18	3	76	6.00		E 396,80	04 N 222	2,517					
Contracto	r	·										Sheet				
Cook Ground Investigation Limited													1 c	of 1		
SAMF	PLES & TE	STS						STRA	TA						ent/	
Depth	Type No	Test Result	Water	Undrained Shear Strength	Legend	Depth (Thick- ness)			DESCF	RIPTION				Geology	Instrument/ Backfill	
- 0.10	D					<u>+ 0.18</u> - 0.35										
0.30	D					- 0.00		MADE GROUND: probable stiff, desiccated, light brown, slightly gravelly CLAY (gravel is brick and glass fragments)							000	
- 0.50	D						CLAY: probable initially firm, light brown to light grey, desiccated CLAY								0000	
- 1.00		N9					0.00 - possible	0.85 - possible relict shear surface (inclined at 45°)							יייי נונונו	
- 1.50	D					- 	1.40 - becomir CLAY, with oc	ng norm casiona	ally hydrate I shell fragr	ed, mottled nents and j	light grey to l bockets of gy	light brown /psum				
- - 2.00 - 2.00	D	N23					2.00 - becomir	ng stiff								
2.50	D					- (4.10) -								CMF		
3.00		N26					3.00 - becomir	ng dark	grey CLAY							
						+ - -										
- 3.50 -	D					-7 	3.65 - weather 3.70 - rootlet c			d						
4.00		N27				- - - - 4.45										
- - -							Core Recovery:									
<u>[_</u>						-	0.0 - 4.0m 100%									
Ē						-	All insitu stren	All insitu strength testing undertaken using CPT								
-						-	Falling head te	Falling head testing carried out								
-						-	Borehole term	inated a	at 4.45m de	pth						
-						- - -	Gas/groundwa with gas valve	ater mor and loc	nitoring star kable cover	idpipe insta	lled to 4.0m	depth; fitte	ed			
- - -						- - -										
-																
-						-										
-						- - -										
	Boring Progress and Water Observations Date Hole Dia.mm Depth Casing Depth Water Depth							iselling	1	Water				RAL		
Date 30/07/2018	Dia. mm	Depth		Depth	Dĩa. mm		- From	То	Hours	From	То		tion s	MARKS		
30/07/2018						DRY	Services d CMF = Ch				cMF = Charm	cted				
												Formation				
		. 1.														
All dimensions in metres Scale 1:50 Client Robert Hitchins Limited Method/ Plant Used Archway Dart 338 Logged By								CN	1							



BOREHOLE LOG

Project									BOREHOLE No					
	akley Farm,	Priors	Road, (Cheltenh	am GL52								52	
Job No		Date										52		
4	360/2		3	0-07-1	8	91	1.00 E 396,896 N 222,409							
Contracto	or											Sheet		
Co	ok Ground	Investi	gation l	imited								1 c	of 1	
SAMPLES & TESTS							STRATA					~	ent/	
Depth	Type No	Test Resu		Undraine Shear Strengtl	Legend	Depth (Thick- ness)			DESC	RIPTION			Geology	Instrument/ Backfill
-						0.30	TOPSOIL: probable firm to stiff, light brown, organic, desiccated, heavily rooted CLAY					esiccated,		
0.30	D					- 0.00	CLAY: prob		light browr	n to light gre	ey, desiccat	ed CLAY		
- 0.50	D				[-			-		-			
- 0.70	D						0.75 - possil	ble shear	surface (in	clined at c4	5°)	to of gunoup		0 0
1.00	D						0.90 - Decor	ning norm		ea, with the	циет роске	ets of gypsum		
1.00 -		N12												Į.
Ē							1.50 - weath	nered fissu	ıre					
-						-	1.80 - becon	ning dark	grey, locall	v mottled lie	ght brown			
2.00		N13							g , ,	,	J			
Ē						(4.15)							CMF	
F														
F					[┝╞╴
- 3.00	D					-	2.90 - becon	ning stiff,	dark bluish	-grey, with	frequent fo	ssil fragments		
3.00		N24												, "E
-					<u> </u>									$ _{o}$
Ē						£								
E					[-								
4.00		N26												
Ē						4.45								-
-						-	Core Recove	ery:						
E						E	0.0 - 4.0m	100%						
Ļ						-								
È						E	All insitu stre	ength test	ing underta	iken using (CPT			
-						-	Borehole ter	minated a	t 4.45m de	pth				
-						-	Gas/ground	water mor	nitoring star	ndpipe insta r	alled to 4.0n	n depth; fitted		
Ē						E	with gas van							
E						E								
-						-								
F						-								
Ē						Ē								
-						-								
F						-								
Ę						E								
L Po	ring Prog		nd W	ator O	beonyoti			hiselling		Water	Addod			
Date	Hole	Depti			ng Dia. mm		From	То	Hours	From	To	GENE REMA		
Dale	Dia. mm	Depu		Depth	Día. mm	Dpt	-	10	TIOUIS	riom	10	Borehole position s		usina
30/07/2018						DRY						Cable Avoidance T services detected	ool (CA	T); no
												CMF = Charmouth	Mudsto	ne
												Formation		
	nsions in m	etres	Client	Robert	Hitchins Lir	mited	Metho Plant I		Arch	way Dart 338		Logged By CN		
S	Scale 1:50 Plant Used Alchiway Dait 358 CM													



Project												BOREH	OLE	No
	akley Farm,			Cheltenha	am GL52							- W	S 3	
Job No			ate				evel (c.m, AOD)		dinates (c.)		1 -			
43 Contracto	360/2		3	0-07-18	5	82	2.00		E 396,94	14 N 22	2,512	Sheet		
		Invotio	otion I	imitod									f 1	
	ok Ground	-		Innited					- •			10	'I I	5
SAM	PLES & TE			Undrained		Depth		STRAT	A				gy	men
Depth	Type No	Test Resul		Shear Strength		(Thick- ness)				RIPTION			Geology	Instrument/ Backfill
F						0.20	TOPSOIL: pr	obable fi	rm to stiff,	dark brown	i, organic, h	eavily rooted		
Ę					<u> </u>	- - -	CLAY: probal	ble initial	ly firm, ligh	nt brown, de	siccated Cl	AY with rare		000
						+ - -	roots 0.65 - possible	e shear s	surface; ra	are gravel o	f rounded m	nedium		000
- - 1.00		N13				} 	limestone 0.90 - becomi	na norm	allv hvdrat	ed. dark gre	ev to liaht br	own CLAY.		
- 1.00						-	with frequent	pockets	of gypsum	, 0	, 0			ł
					F									
-						- -								ł
- 2.00		N18				- - -								
						(4.25)							CMF	
-						-	2.60 - no mor	o livo roc	tlata abaa	aved				
F						- - -	2.00 - 110 1101			veu				
3.00		N23				+- - -	3.00 - becomi	ng stiff						
-						-								
F						F	3.50 - frequer	nt fossil f	ragments					ľĒ
-					<u> </u>	- - -								
4.00		N28			<u> </u>	-1 -F								
Ę						4.45								-
E						-	Core Recover	y:						
-						-	0.0 - 4.0m 1	00%						
F.						-	All insitu stren	igth testi	ng underta	ken using (CPT			
-						-	Borehole term	-	•	•				
-						-	Gas/groundwa with gas valve	ater mon and locl	itoring star kable cove	ndpipe insta r	lled to 4.0n	n depth; fitted		
F						-								
-						-								
Ē						-								
-						-								
F														
						-								
-						-								
Во	oring Progress and Water Observations Chiselling Water Added GENERAL													
Date	Hole Dia. mm	Depth		Casir epth I	ig Dia. mm	Water Dpt	From	То	Hours	From	То	REMA		
30/07/2018						DRY						Borehole position s Cable Avoidance T services detected	canned ool (CA	l using T); no
												CMF = Charmouth	Mudsto	ne
												Formation		
	nsions in m	etres	Client	Robert	Hitchins Lir	nited	Method/		Δreb	way Dart 338		Logged By CM		
S	cale 1:50			Robert	Internitio Ell	inteu	Plant Us	sed	Aich	way Dalt 330				



Project	klov Form	Driore D	ood Cl	holtonha	m CI 52	540						BOREH	OLE	No
Job No	akley Farm,	Da					evel (c.m, AC	D) Co-Oi	dinates (c.))		- W	54	
4:	360/2		30	-07-18			4.00		E 397,04		2,516			
Contracto	or											Sheet		
Co	ok Ground	Investiga	ation Li	mited								1 0	f 1	
SAMF	PLES & TE	STS			1	1		STRA	ТА				×	ient/
Depth	Type No	Test Result	at l	Undrained Shear Strength	Legend	Depth (Thick- ness)			DESCI	RIPTION			Geology	Instrument/ Backfill
E						(0.40) 0.40	MADE GRO GRAVEL (g	OUND: gravel is br	ass over pro	obable med crete)	ium dense,	sandy		
-						2 0.40 	CLAY: prot			•	AY			
- 1.00		N11				- - - - - -	4.50 have							
2.00		N16					1.50 - becompockets of c	ming mott crystalline	led light bro gypsum	wn to light	grey, with f	requent		
- - - - -						- - (4.05) -	2.50 - beco	ming dark	grey CLAY				CMF	
3.00		N20				+ - - - - - - - - - -	3.00 - beco	ming stiff						
4.00		N28				- 								
-						4.45	Core Recov	very:						_
-						-	0.0 - 4.0m	100%						
-						-	All insitu str	ength test	ing underta	ken using (CPT			
-						-	Borehole te	rminated a	at 4.45m de	pth				
- - - -						-	Gas/ground with gas val	lwater mor ve and loc	nitoring star kable cove	ndpipe insta	lled to 4.0r	n depth; fitted		
-						-								
-						-								
- - - -														
E						-	++							
	ring Prog Hole					Water		Chiselling To	1	Water	Added To	GENE REMA		
Date 30/07/2018	Dia. mm	Depth	De	Casin epth [Día. mm	Dpt	- From	10	Hours	From	10	Borehole position s Cable Avoidance To services detected	canned	using
												CMF = Charmouth Formation	Mudstor	ne
	nsions in m cale 1:50	etres (Client	Robert H	litchins Lin	nited	Metho Plant		Arch	way Dart 338		Logged By _{CM}		





WS1-core 0.0-4.0m



WS1 – possible shear plane at 0.85m



WS2 - core 0.0 - 4.0m



WS3 - core 0.0 - 4.0m



WS4 - core 0.0 - 4.0m



Project													BOREH	IOLE	No
0	akley Fa	arm, Pr	iors Ro	ad, C	heltenh	am GL52							- w	S5	
Job No			Dat					evel (c.m, AOD)		dinates (c.)				00	
4	360/2			30	0-07-18	8	94	4.00		E 397,17	8 N 22	2,509			
Contracto	or												Sheet		
Co	ook Gro	und Inv	/estigat	tion L	imited								1 (of 1	-
SAM	PLES 8	TEST	S						STRAT	Ā					ent/
Depth			Test Result	Water	Undraine Shear Strength	Legend	Depth (Thick- ness)				RIPTION			Geology	Instrument/ Backfill
- - 0.10 - 0.25							<u>- 0.15</u> - 0.40	rooted CLAY		-			/		_
0.20								MADE GROU	ND (rew AY, with	orked): pro	obable firm of charco	i to stiff, light al	brown,	/	1
- 1.00			N10					CLAY: probab CLAY, with rar 0.65 - possible 0.90 - becomin	ole initial re round e shear s	ly firm, ligh ed limestor surface	t brown to ne and rare	light grey, de	siccated		
2.00		D						1.50 - no roots	s observe	ed below th	is depth				
2.00			N13				(4.05)							CMF	
3.00			N14					2.80 - becomir gypsum	ng dark (grey CLAY,	with rare	pockets of cr	ystalline		
4.00			N29				4.45	4.00 - becomir	ng stiff						_
-							- - -	Core Recovery	y:						
<u> </u>							-	0.0 - 4.0m 10	00%						
							Ē	All insitu stren	gth testi	ng underta	ken using	CPT			
- - - -							- - - -	Borehole termi completion of t	inated at testing a	t 4.45m de Ind samplir	oth; backf Ig	illed with aris	ing upon		
-															
							- - -								
							- 								
+ - -							- - -								
-							- - -								
Во			ss and			oservati		Ch	iselling		Water	Added	GENE		
Date	Hole Dia. m		Depth	D	Casi epth	ng Dia. mm	Water Dpt	From	То	Hours	From	То	REMA		
30/07/2018							DRY						Borehole position Cable Avoidance services detected	scanned Tool (CA	using T); no
													CMF = Charmouth Formation	Mudsto	ne
All dime			es C	lient	Robert	Hitchins Lir	nited	Method/ Plant Us		Archv	vay Dart 338		Logged By	1	
S	cale 1:	50													



Project												BOREH	OLE	No
Oal	kley Farm,	Priors F	Road, (Cheltenha	am GL52							- w	22	
Job No		D	ate				evel (c.m, AC	DD) Co-Or	dinates (c.)				50	
	360/2		3	0-07-18	3	10	3.00		E 397,29	99 N 22	2,490			
Contractor												Sheet		
	ok Ground	Investig	ation I	_imited								1 c	ot 1	1
SAMF	PLES & TE	STS				5 //		STRA	TA				λf	nent
Depth	Type No	Test Resul		Undrained Shear Strength	Legenc	Depth (Thick- ness)				RIPTION			Geology	Instrument/ Backfill
-						(0.40) 0.40	heavily root	ted CLAY		-	n, organic, o			0 0
0.50	D						CLAY: pro	bable initia	Illy stiff and	friable, ligh	it brown, des	siccated CLAY		
- - 1.00 - 1.00	D	N11					0.90 - becc	oming firm,	normally h	ydrated, mo	ottled light bi	rown and grey		
- 1.50	D													
- - 2.00 - 2.00	D	N16											0145	
2.50	D					_ (4.05) 							CMF	
- 3.00 - 3.00	D	N20					3.00 - becc	ming stiff						
4.00		N32												
-						4.45								-
t L						-	Core Reco	-						
-						-	0.0 - 4.0m	100%						
F						-	All insitu st	rength test	ing underta	ken using	CPT			
Ē						-	Falling hea	d testing ca	arried out					
-						-	Borehole te	erminated a	at 4.45m de	pth				
-						Borehole terminated at 4.45m depth Gas/groundwater monitoring standpipe installed to 4.0n with gas valve and lockable cover					n depth; fitted			
- - -						- - -								
- - -						- -								
-						-								
-														
Bor	ing Prog	ress a						Chiselling)	Water	Added	GENE		
Date	Hole Dia. mm	Depth	ו	Casir Depth [ig Dia. mm	Water Dpt	From	То	Hours	From	То	REMA	RKS	
30/07/2018						DRY						Borehole position s Cable Avoidance T services detected	canned ool (CA	using T); no
												CMF = Charmouth Formation	Mudsto	ne
	sions in m cale 1:50	etres	Client	Robert I	Hitchins Lir	nited	Meth Plant	od/ Used	Arch	way Dart 338	·]	Logged By _{CM}		



Project														BOREH	OLE	No
Oa	kley Farm	n, Prio	ors Ro	ad, C	heltenha	am GL52	5AQ							\٨/	S7	
Job No			Date	е			Ground Le		, aoe	D) Co-Or	dinates (c.))		VV	51	
4:	360/2			30	0-07-18	3	10	1.00			E 397,14	0 N 22	2,423			
Contracto	or													Sheet		
Co	ok Groun	d Inve	estigat	ion L	imited									1 c	of 1	
SAMF	PLES & T	ESTS			_					STRAT	ГА				/	ent/
Depth	Type No	T Re	est esult	Water	Undrained Shear Strength	Legend	Depth (Thick- ness)				DESC	RIPTION			Geology	Instrument/ Backfill
							0.25	TOPSO	DIL: p	probable s	tiff, light br	own, organ	iic, desiccate	d, heavily		
								rooted (CLAY: grey CL	proba		lly firm to si	tiff, desicca	ated, light bro	own to light		
- 1.00		1	N8					1.00 - b	econ	ning soft t	o firm, norr	mally hydra	ted			
- 2.00		N	124				- (3.20) 	2.00 - b	ecom	ning stiff					CMF	
3.00		N	150					2.80 - 1	0mm	n band of i	iron-rich lin	nestone				
E							3.45									-
-							-	Core Recovery:								
-							-	0.0 - 4.0	0m	100%						
F							-	All insitu	u stre	ength testi	ing underta	ken using	СРТ			
-							-	Borehol	le terr	minated o	n iron-rich pletion of te	limestone a	at 3.45m dep sampling	oth; backfilled		
							-	With Cirk	onig t				ouriping			
-							-									
							-									
-							-									
F							-									
Ľ							-									
-							-									
Ľ							-									
-							-									
Ę							-									
			0.000	1 / / /	l ator Oh			11	~	hicolling		\A/otor	Added	051/5		
Date	ring Pro Hole Dia. mm	1	epth		Casir Casir	ng Dia. mm	Water Dpt	From		hiselling To	Hours	From	To	GENE REMA		
30/07/2018							DRY							Borehole position s Cable Avoidance T services detected	canned ool (CA	using T); no
														CMF = Charmouth Formation	Mudsto	ne
	nsions in r cale 1:50	netres	s C	lient	Robert	Hitchins Lir	nited		lethoo lant L		Arch	 way Dart 338		Logged By _{CN}		



Project												BOREH	OLE	No
Oa	kley Farm,	, Priors I	Road,	Cheltenh	am GL52	5AQ						\\/	S 8	
Job No			ate				evel (c.m, AOD)		inates (c.)			•••	50	
	360/2		3	31-07-1	8	96	6.00	E	E 397,01	6 N 22	2,419			
Contracto	or											Sheet		
Co	ok Ground	l Investig	gation	Limited								1 0	of 1	
SAME	PLES & TE	STS						STRAT	A				~	ent/
Depth	Type No	Test Resu		Undraine Shear Strength	Legend	Depth (Thick- ness)			DESCF	RIPTION			Geology	Instrument/ Backfill
- 0.10	D					0.30	TOPSOIL: pro rooted CLAY	obable fir	m, light br	own, orgai	nic, desiccate	d, heavily		
0.30	D					-	CLAY: probat	ole initially	y stiff, des	iccated, lig	ht brown to li	ght grey		
- 0.50	D						CLAY, with oc	casional	gravel of s	subangular	Imestone			000
- 0.80-0.90 - 1.00) D	N111				1 +-	1.00 boomi	na firm						
-		N11					1.00 - becomir	-						
- 1.30	D					·	1.30 - appearii	ng norma	ally hydrate	ed				
-						-								₽
- 2.00	D													
2.00		N16			<u> </u>									
2.30	D					- (4.15)	2.50 - weather	rod ficcur	e observe	d: becomi	na stiff dark	arev with	CMF	
-						1	relict mudston	e structu	re evident		ng sun, uark	grey, with		
- 3.00		N26												
-														
- 3.30	D													
-														ŀ₽
- 4.00		N27				· [·]								Ì- IÌ-
						- 4.45								
-						-	Core Recovery	N.C.						1
F						-	-							
						Ē	0.0 - 4.0m 10							
-						E	All insitu stren	-	-	-	CPT			
-							Borehole term							
-						-	Gas/groundwa with gas valve	ater monif	toring stan able cover	idpipe inst	alled to 4.0m	depth; fitted		
-						È								
-						F								
E .						E								
E						E								
-						Ē								
Ē						Ē								
-						-								
Boi	ring Prog	ress a	nd W	/ater Ol	oservati	ons	Ch	iselling		Water	Added	GENE	RAI	
Date	Hole Dia. mm	Depth		Casi Depth			From	То	Hours	From	То	REMA		
04/07/02/12					, , , , , , , , , , , , , , , , ,							Borehole position s Cable Avoidance T	scanned	using
31/07/2018						DRY						services detected		r), no
												CMF = Charmouth Formation	Mudsto	ne
	nsions in m	etres	Client	t Robert	Hitchins Li	mited	Method/ Plant Us		Archv	vay Dart 338		Logged By CN	1	
S	cale 1:50						Plant US	seu						



Project														BC)REF	IOLE	No
Oa	akley Farn	n, Prio	rs Ro	ad, C	heltenha	am GL52	5AQ								\٨/	S 9	
Job No			Date	е			Ground L		m, AC	D) Co-Or	dinates (c.))			vv	39	
43	360/2			3	1-07-18	3	11	0.00			E 397,23	89 N 22	2,402				
Contracto	or													Shee	et		
Co	ok Groun	d Inve	stigat	ion L	imited										1 (of 1	
SAM	PLES & T	ESTS								STRA	ТА						ent/
Depth	Type No	e T Re	est sult	Water	Undrained Shear Strength	Legend	Depth (Thick- ness)					RIPTION				Geology	Instrument/ Backfill
							0.30	TOPS	SOIL:	probable f ed CLAY	irm to stiff,	dull brown	, organic, de	siccated,			
- 0.20	D							CLAY	: prol		lly stiff, ligh	t brown to	light grey, de	esiccated			
0.50	D						1 -	CLA	(
- 0.70	D						£										
1.00		N	12					1.10	- beco	mina firm.	normally h	vdrated. lia	ht brown to	liaht arev			
- 1.30	D					<u> </u>					l of subrou						
Ē																	
- 1.70	D						(3.14)									CMF	
2.00		N	24				Ē	2.00	- beco	ming stiff							
2.30	D																
F						<u> </u>	+										
2.70	D						f										
- 3.00			50/				1 +	2.90 evide		ng to dark	grey CLAY	, with relict	mudstone	structure			
E		295	mm			[3.44										
F							-	Core Recovery:									
E							Ē			-							
F							-	0.0 -	3.0m	100%							
F							Ę	All in:	situ str	rength test	ing underta	ken using	СРТ				
Ę							Ę	Fallin	a head	d testing ca	arried out						
-							-		-	•		+ 2 11m do	nth: hookfill	od with			
E							F				ion of testir		pth; backfill pling	ed with			
F							Ę										
Ē							Ē										
F							-										
F							-										
Ē							E										
F							-										
							Ē										
-							-										
E							Ē										
Ę							E										
F							-										
[-										
Во	ring Pro	gress	s and	d Wa	ater Ob	servati	ons		(Chiselling)	Water	Added		GENE		
Date	Hole Dia. mm	De	epth	D	Casir epth	ng Dia. mm	Water Dpt	Fr	om	То	Hours	From	То	F	REMA	RKS	
31/07/2018							DRY							Borehole p Cable Avo	idance 7	scanned Fool (CA ⁻	using T); no
														services d		Mudsto	ne
														Formation			-
								<u> </u>									
	nsions in i cale 1:50	netres		lient	Robert	Hitchins Lir	nited		Metho Plant		Arch	way Dart 338		Logged	By _{CN}	Л	





WS5 - core 0.0 - 4.0m



WS5 – possible shear plane at 0.65m



WS6 - core 0.0 - 4.0m



WS7 - core 0.0 - 3.0m



WS8 - core 0.0 - 3.0m



WS9 - core 0.0 - 4.0m

SPT Calibration Report



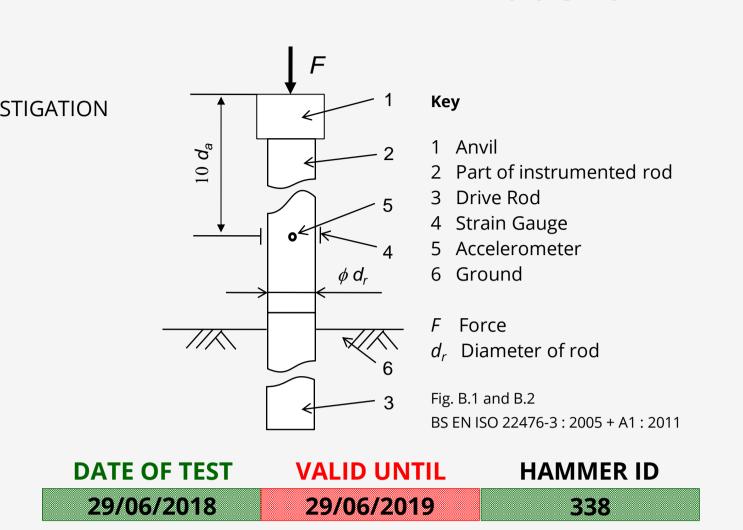
www.equipegroup.com

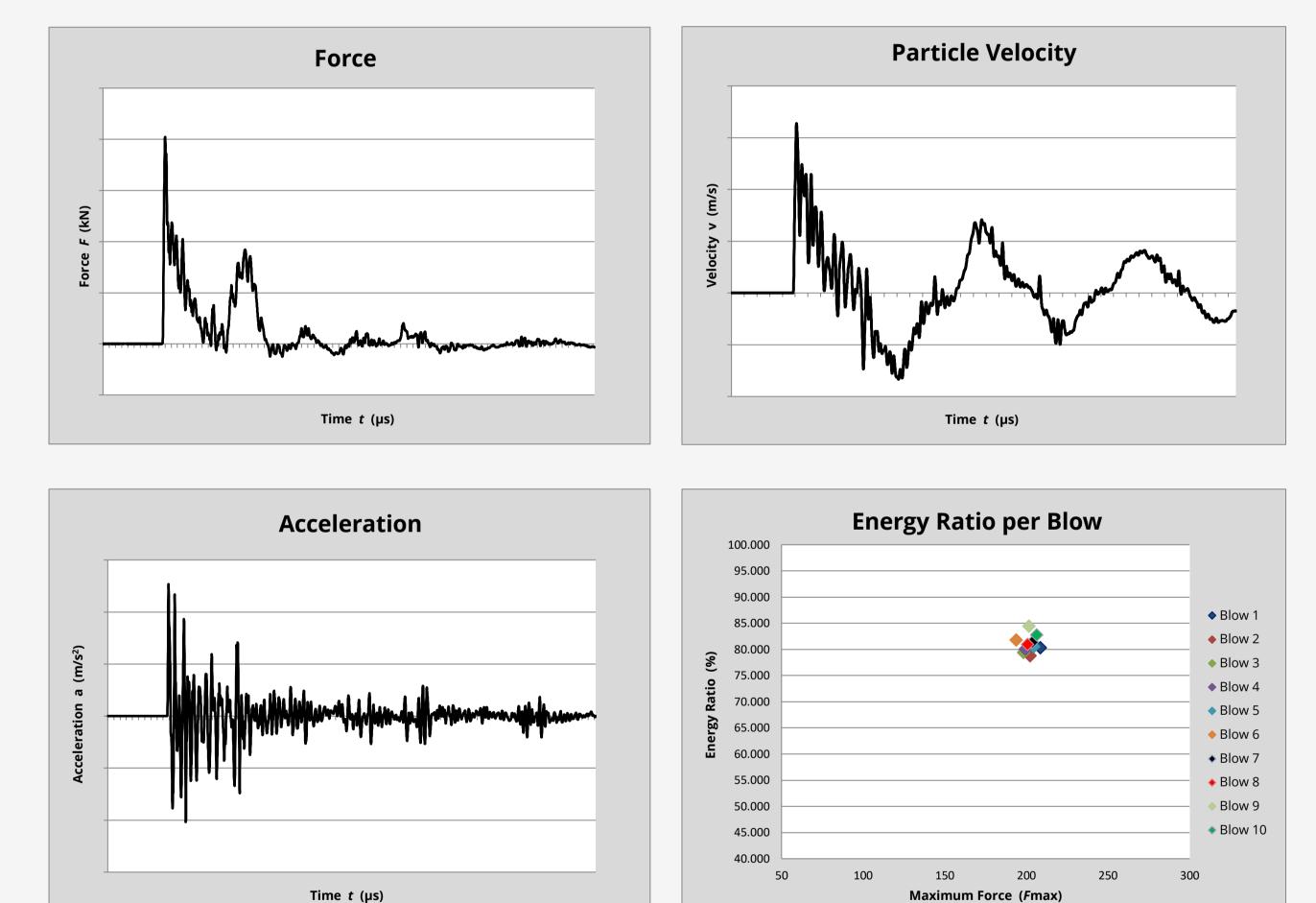
Hammer Energy Measurement Report

Type of Hammer		DART
Client		COOK GROUND INVES
Test No		EQU2109
Test Depth (m)		8.70
Mass of hammer	<i>m</i> =	63.5kg
Falling height	h =	0.76m
E _{theor} =	m x g x h =	473J

Characteristics of the instrumented rod

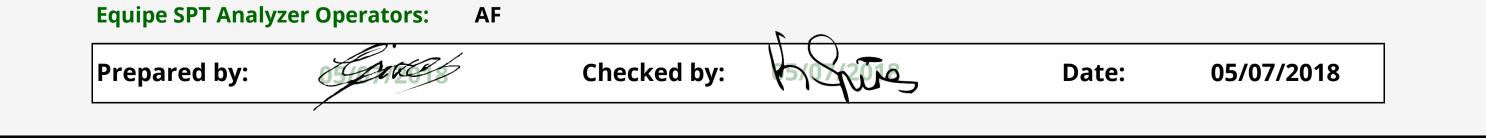
Diameter	<i>d</i> _r = 0.052 m
Length of instrumented rod	0.558 m
Area	A = 11.61 cm ²
Modulus	<i>E_a</i> = 206843 MPa





Time t (µs)

Observations: 1. E meas = 0.382 kN-m **E**_{meas} Energy Ratio = *(E*_r) 80.75% E theor = **0.473** kN-m \pmb{E}_{theor} © Copyright 2018



Equipe Group, The Paddocks, Home Farm Offices, The Upton Estate, Banbury, Oxfordshire, OX15 6HU © Copyright 2018 Fax: +44 (0)1295 678232 Tel: +44 (0)1295 670990 Email: info@equipegroup.com



Project												BOREH	OLE	No
Oa	akley Farm,	Priors	Road, (Cheltenha	am GL52	5AQ						\\/<	510	
Job No			Date			Ground L	evel (c.m, AOD)) Co-Orc	dinates (c.)			VVC	510	
4	360/2		3	0-07-18	В	11	8.00		E 397,09	0 N 22	2,249			
Contracto	or											Sheet		
Co	ook Ground	Investi	gation I	imited								1 0	of 1	
SAM	PLES & TE	STS						STRAT	A					ent/
Depth	Type No	Test Resu		Undrained Shear Strength	Legend	Depth (Thick- ness)			DESCF	RIPTION			Geology	Instrument/ Backfill
0.05	D					0.20	TURF over TO sandy CLAY,	OPSOIL:	probable f	irm, dark	brown, organ	ic, slightly		Ш
0.20 0.50	D					0.50		ble firm to	o stiff, brov	vn mottlec	l orange and ss rootlets, s	grey, silty, lightly	CMF	
- 1.00		N23	;			1.00			-			/		
1.50	D					(1.40)	1.00 - slightly coarse, extrem 1.20 - becomin	gravelly onely weal	(gravel is a k mudstone	ngular to : e)	subangular, r	nedium and	CMF	
- 2.00		N46	;			2.40	brown, very sil 1.65 - gravel b 1.85 - very thiu (iron) on bedd	Decoming nly bedde	g very weak ed, grey, si	c Ity CLAY,	weathered or	angish-brown		
						2 2 2 2 2 (1.02)	2.00 - becomin CLAY/MUDST reddish-brown	ng very s TONE: p	stiff probable ve			nottled	CMF	
3.00		N50/ 267 m			× × ×	3.42								_
-						-	Core Recovery	y:						
-						Ē	0.0 - 3.0m 10	00%						
-						F	All insitu stren	ath tectiv	na undertal	kon usina	SDT			
Ē						E		0	0	0	JF I			
-						Ę	Borehole term	inated at	t 3.42m dej	pth				
- - - -						- - - -	Gas/groundwa with gas valve	ater moni and lock	itoring stan kable cover	idpipe inst	alled to 3.0m	depth; fitted		
- - - -						- - - -								
- - - -						- - - -								
- - - -						- - - -								
- - - -						-								
- - - -						- - - -								
-						-								
Во	ring Prog	ress a					Ch	iselling		Water	Added	GENE	RAL	
Date	Hole Dia. mm	Dept	h [Casii Depth	ng Dia. mm	Water Dpt	From	То	Hours	From	То	REMA		
30/07/2018						DRY						Borehole position = Cable Avoidance T services detected	ool (CA	T); no
												CMF = Charmouth Formation	Mudsto	ne
	nsions in m	letres	Client	Robert	Hitchins Li	mited	Method/ Plant Us		indow Sampli	ing / Terrier 2	11 2002 (T06)	Logged By AJ		



Project					o						BOREH	OLE	No
Oa Job No	akley Farm,	Priors Ro		Cheltenha	am GL52		avel (c m AOD)	Co-Ordinates (c)		WS	511	
	360/2	Da		0-07-18	2		9.00		.) 06 N 222,30	Δ			
Contracto			0	0-07-10	,		0.00	L 007,0	00 11 222,00		Sheet		
Co	ook Ground	Investiga	tion L	imited							1 0	f 1	
	PLES & TE							STRATA					nt/
Depth	Туре	Test	Water	Undrained Shear		Depth (Thick-			RIPTION			Geology	Instrument/ Backfill
	No	Result	3	Strength	XXXXX	ness)				<u>.</u>		Ge	Ba
- 0.00-0.30 - 0.10 -						* 0.20 - - 0.55	gravelly, desice to coarse mud	PSOIL: probable cated CLAY (grav stone, chalk, occa	el is subangular t	o subrou	nded, fine		
0.50	D				<u>xo_ x</u>	<u>- 0.55</u> ≯		nt grass rootlets ble firm, greyish-bi	own verv sandv	slightly	navelly		
0.75	D					+ }	CLAY (gravel i	is angular to subro	bunded, fine to co	arse mu	dstone);		010
- 1.00		N11			× ×	+	occasional roo CLAY: firm, g	rey mottled orang	e and brown, silty	, slightly	sandy,		
Ę					× · · · · · · · · · · · · · · · · · · ·		slightly gravelly medium muds	y CLAY (gravel is	angular to subrou	inded, fir	ne to		
					X X	(2.15)	1.35 - becomir					CMF	ļ
[1.75 - 2.00	D	NOF			×°X	≯ ↓	2.00 boomir	ag atiff					
- 2.00		N25				<u>}</u> +	2.00 - becomir	ig suit					
						÷ > - 270							
-						<u> </u>	CLAY/MUDST	ONE: very stiff, o	prange and greyis	h-brown	mottled red,		†₽
- 3.00		N36			× ~~× ~	(0.65)	thinly laminate MUDSTONE	d, silty, slightly gra	avelly CLAY/extre	mely we	ak	CMF	l d
						3.35	01.437	::::::::::::::::::::::::::::::::::::::	×				
-						≯ -	CLAY: Very st	iff, grey, silty CLA	Υ				
Ę					× ×	 ≯ (1.06)						CMF	
4.00		N50/				L`´´							
-		291 mm	1		×	4.41							-
-						-	Core Recovery	<i>/</i> :					
- - - -						- - -	0.0 - 1.2m ha 1.2 - 4.0m 10	and-dug starter pit 0%					
-						-	All insitu stren	gth testing undert	aken using SPT				
Ę						-	Borehole term	inated upon refus	al at 4.41m depth	1			
						-	Gas/groundwa	ater monitoring sta	ndpipe installed t		epth; fitted		
-						-	with gas valve	and lockable cove	er				
E C						-							
-						-							
F						-							
Ē						-							
						-							
						-	11		4				
Bo	ring Prog		d Wa				Ch	iselling	Water Add		GENE		
Date	Hole Dia.mm	Depth		epth [ig Dia. mm	Water Dpt	From	To Hours	From T		REMA		
30/07/2018						DRY				C	orehole position s able Avoidance T ervices detected		
											MF = Charmouth	Mudsto	ne
										F	ormation		
	nsions in m	etres (Client	Robert I	Hitchins Lir	nited	Method/ Plant Us		l l bling / Terrier 2002 (T	L	.ogged By _{AJ}		
S	cale 1:50												



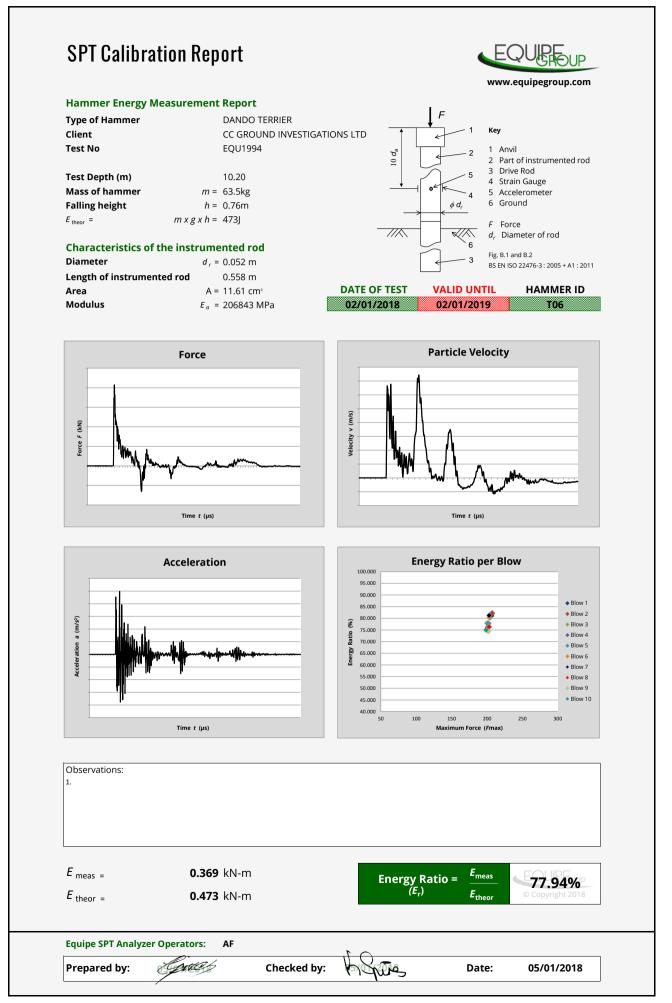


WS10 - core 1.0 - 3.0m

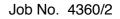
WS10a



WS11 - core 1.0 - 3.0m



© Copyright 2018 Equipe Group, The Paddocks, Home Farm Offices, The Upton Estate, Banbury, Oxfordshire, OX15 6HU Tel: +44 (0)1295 670990 Fax: +44 (0)1295 678232 Email: info@equipegroup.com





APPENDIX 2

CONTAMINATION STATUTORY FRAMEWORK / METHODOLOGY AND CERTIFIED CONTAMINATION TEST RESULTS



A2 CONTAMINATION RISK ASSESSMENT

Statutory Framework

- A2.1 Part 2A of the Environmental Protection Act 1990 (inserted by Section 57 of the Environment Act 1995) provides a regime for the control of specific threats to health or the environment from existing land contamination. In accordance with the Act and the statutory guidance document on the Contaminated Land (England) Regulations 2000, the definition of contaminated land is intended to embody the concept of risk assessment. Within the meaning of the Act, land is only 'contaminated land' where it appears to the regulatory authority, by reason of substances within or under the land, that:
 - Significant harm is being caused or there is significant possibility of such harm being caused; or
 - Pollution of controlled waters is being, or is likely to be, caused.
- A2.2 In 2012 revised Statutory Guidance for Part 2A of the Environmental Protection Act (1990) came into force for England and Wales. This introduced a new four category approach for classifying land affected by contamination to assist decisions by regulators in cases of Significant Possibility of Significant Harm (SPOSH) to specified receptors, including humans, and significant pollution of controlled waters.

Category 1 describes land which is clearly problematic e.g. because similar sites are known to have caused a significant problem in the past. The legal definition is where "there is an unacceptably high probability, supported by robust science-based evidence, that significant harm would occur if no action is taken to stop it".

Categories 2 and 3 cover land where detailed consideration is needed before deciding whether it may be contaminated land. Category 2 is defined as land where "there is a strong case for considering that the risks from the land are of sufficient concern that the land poses a significant possibility of significant harm". Category 3 is defined as land where there is not the strong case described in the test for Category 2, and may include "land where the risks are not low, but nonetheless the authority considers that regulatory intervention under Part 2A is not warranted". The decision basis is initially related to human health risks, and if this is not conclusive due to uncertainty over risks, wider socio-economic factors (e.g. cost, local perception etc).



Category 4 describes land that is clearly not contaminated land, where there is no risk or the level or risk posed is low.

This same 4 category system has also been introduced to assist in identifying whether there is a significant possibility of significant pollution of controlled waters. Part 2A states that normal levels of contaminants in soil should not be considered to cause land to qualify as contaminated land, unless there is a particular reason to consider otherwise.

Following publication of the revised Statutory Guidance, DEFRA commissioned a research project to develop new Category 4 Screening Levels (C4SLs) to provide a simplified test for regulators to aid decision-making on when land was suitable for use and definitely not contaminated land under the statutory regime. The output from this research project was published by CL:AIRE in December 2013, with Policy Companion Documents published in England by DEFRA in March 2014 and the Welsh Government in May 2014. The culmination of this work was the development of a framework and methodology for deriving C4SLs and the publication of final C4SLs for use as new screening values for six common contaminants.

Further research by LQM on behalf of CIEH lead to the publication in 2015 of the Suitable for Use Levels known as S4ULs, and these are now widely adopted as a robust and authoritative source of guidance (see A2.14 below).

Once land has been determined as contaminated land, the enforcing authority must consider how it should be remediated and, where appropriate, it must issue a remediation notice to require such remediation. The enforcing authority for the purposes of remediation may be the local authority which determined the land, or the Environment Agency which takes on responsibility once land has been determined if the land is deemed to be a "special site". The rules on what land is to be regarded as special sites, and various rules on the issuing of remediation notices, are set out in the Contaminated Land (England) Regulations 2006

A2.3 The UK guidance on the assessment of land contamination has developed as a direct result of the introduction of the above two Acts. The technical guidance supporting the new legislation has been summarised in a number of key documents collectively known as the Contaminated Land Reports (CLRs), a proposed series of twelve documents. Seven were originally published in March 1994, four more were published in April 2002, while the last remaining guidance document (CLR 11 was published in



2004. In 2008 CLR reports 7 to 10 were withdrawn by the Department of Environment Food & Rural Affairs and the Environment Agency and updated versions of CLR 9 and 10 were produced in the form of Science Reports SR2 and SR3.

- A2.4 The guidance defines 'risk' as the combination of:
 - The probability, or frequency, of occurrence of a defined hazard (e.g. exposure of a property to a substance with the potential to cause harm); and
 - The magnitude (including the seriousness) of the consequences.
- A2.5 For a risk of pollution or environmental harm to occur as a result of ground contamination, all of the following elements must be present:
 - A source, i.e. a substance that is capable of causing pollution or harm;
 - A pathway, i.e. a route by which the contaminant can reach the receptor; and
 - A receptor (or target), i.e. something which could be adversely affected by the contaminant.
- A2.6 If any one of these elements is missing there can be no significant risk. If all are present then the magnitude of the risk is a function of the magnitude and mobility of the source, the sensitivity of the receptor and the nature of the migration pathway.
- A2.7 The presence of contamination is also a material issue in the determination of planning applications, and where a change of use is proposed, especially on brownfield (former industrial) land, investigation, assessment and remediation of contamination is often a requirement of the Planning Authority. The presence of contamination may consequently require remedial action prior to redevelopment, in circumstances which would otherwise be unlikely to result in the determination of the land as contaminated land as defined in the above legislation.

Contamination Assessment Methodology

A2.8 The guidance proposes a four-stage assessment process for identifying potential pollutant linkages on a site. These stages are set out in the table below:



No.	Process	Description
1	Hazard Identification	Establishing contaminant sources, pathways and receptors (the preliminary conceptual site model).
2	Hazard Assessment	Analysing the potential for unacceptable risks (what linkages could be present, what could be the effects).
3	Risk Estimation	Trying to establish the magnitude and probability of the possible consequences (what degree of harm might result and to what receptors, and how likely is it).
4	Risk Evaluation	Deciding whether the risk is unacceptable.

- A2.9 Stages 1 and 2 develop a *'preliminary conceptual model'* based upon information collated from desk studies and usually a site walkover inspection. The formation of a conceptual site model is an iterative process, and it should be updated and refined throughout each stage of the project to reflect any additional information obtained.
- A2.10 The information gleaned from the desk studies and associated enquiries is presented in a desk study report with recommendations, if necessary, for further work based upon the preliminary conceptual site model. CLR 8, together with specific DoE 'Industry Profiles' provides guidance on the nature of contaminants relating to specific industrial processes. Whilst it is acknowledged that CLR 8 has been withdrawn no replacement guidance has yet been published that lists the contaminants likely to be present on contaminated sites, thus CLR 8 guidance is still considered relevant.
- A2.11 If the preliminary conceptual model identifies potential pollutant linkages, a Phase 2 site investigation is normally recommended, unless appropriate mitigation measures can be incorporated into the proposed development sufficient to negate the identified risks, subject to local planning authority approval. The number of exploratory holes and samples collected for analysis should be consistent with the size of the site and the level of risk envisaged. This will enable a contamination risk assessment to be conducted, at which point the preliminary conceptual model can be updated and relevant pollutant linkages identified.

Preliminary Risk Assessment

A2.12 By considering the various potential sources, pathways and receptors, a preliminary assessment of potential risk is made based upon the likelihood of the occurrence and the severity of the potential consequence, the latter being a function of the sensitivity



of the receptor. At Phase 1 desk study stage the qualitative risk assessment is based on the categories tabulated below.

Category	Definition
Severe	Acute risks to human health, catastrophic damage to buildings/property, major pollution to controlled waters
Moderate	Chronic risk to human health, pollution of sensitive controlled waters, significant effects on sensitive ecosystems or species, significant damage to buildings or structures
Mild	Pollution of non-sensitive waters, minor damage to buildings or structures
Minor	Requirement for protective equipment during site works to mitigate health effects, damage to non-sensitive ecosystems or species

A2.13 The likelihood of an event (probability) takes into account both the presence of the hazard and receptor and viability of the pathway, and is based on the categories tabulated below.

Category	Definition
Highly likely	Pollutant linkage may be present, and risk is almost certain to occur in long term, or there is evidence of harm to the receptor
Likely	Pollutant linkage may be present, and it is probable that the risk will occur over the long term
Possible	Pollution linkage may be present, and there is a possibility of the risk occurring, although there is no certainty that it will do so
Unlikely	Pollutant linkage may be present, but the circumstances under which harm would occur are improbable

A2.14 On this basis potential hazards are assigned a risk rating as shown below.

			Consequence		
		Severe	Moderate	Mild	Minor
Probability	Highly likely	very high	high	moderate	low
Probability (Likelihood)	Likely	high	moderate	low/moderate	low
	Possible	moderate	low/moderate	low	very low
	Unlikely	low/moderat e	low	very low	very low



- A2.15 At Phase 2 stage, quantitative assessment of human health risk posed by ground contamination is achieved by comparison of soil concentrations with Tier 1 Category Four Screening Levels (C4SL) published by DEFRA (2014), and/or Suitable for Use Levels (S4UL) as published by LQM/CIEH (2015). The official Soil Guideline Values utilise a soil organic matter content of 6% which is considered to be higher than typical UK soils, however three sets of S4UL's have been developed for organic matter contents of 1%, 2.5% and 6%, thus the most appropriate set is selected based upon proven site conditions.
- A2.16 Contaminant concentrations below the threshold screening values are considered not to warrant further risk assessment. Concentrations of contaminants above these screening values require further consideration of potential pollutant linkages and may indicate potentially unacceptable risks to site users. Such exceedances may trigger a Tier 2 detailed quantitative risk assessment (DQRA) where site-specific parameters are used to derive site specific assessment criteria (SSAC), usually by using the CLEA Model (V1.06 at time of writing). It should be noted that exceedance of a screening value does not necessarily indicate that the site requires remediation.
- A2.17 In order to assess any risk to controlled waters posed by contaminants within the underlying soils and groundwater, laboratory results have been screened against Level 1 Environmental Quality Standard (EQS) values derived from the Water Framework Directive (Standards & Classification) Directions (England & Wales) 2015 and the current UK Drinking Water Supply (Water Quality) Regulations (DWS), dependent upon the most vulnerable receptor. The EQS is usually an upper concentration set for the receiving watercourse and not the discharge itself. The DWS is established for compliance at the point of use or abstraction and not the source area.



SUMMARY OF CONTAMINATION TESTING RESULTS

_

									SOIL	S									L	EACHA	TES					
	E					тохіс	META	L S (mg/k	g)			DTOXIC LS (mg/kg)	(%)	(%				тохіс	META	LS (µg/l)				DTOXIC		
Sample Ref	Sample Depth	Sample of	Hd	Arsenic	Cadmium	Chromium III	Lead	Meraury	Selenium	Nickel	Copper	Zinc	Moisture @ 105C (?	Soil Organic Matter (%)	Asbestos Screen	Arsenic	Cadmium	Chromium	Lead	Mercury	Selenium	Nickel	Copper	Zinc		
WS1	0.1	topsoil (clay)	5.9	22	1	35	190	<1	<3	32	41	190	23		<u>i</u>			<u>.</u>		<u>i</u>						
WS1	0.3	made ground (clay)	6.6	21	<1	43	79	<1	<3	31	23	100	18	·····	÷		h	÷				·····		*	CIEH/LQM	s= GAC/S4UL presented exceeds the solubility saturation limit, which is presented in brackets
WS2	0.3	CMF (clay)	6.0	16	<1	42	27	<1	<3	35	21	100	16	÷	<u>.</u>		[*****	CIEH/LQM	v = GAC/S4UL presented exceeds the vapour saturation limit, which is presented in brackets
WS2	0.5	CMF (clay)	6.3	15	<1	53	32		<3	33		94	20	1.0			<u>}</u>		<u>.</u>						-	S4UL based on a threshold protective of direct skin contact with phenol (guideline in brackets
WS3	0.15	topsoil (clay)	5.9	16	<1	37	110	<1	<3	26	23	130	27		<u>.</u>	0.3	<0.02	9	0.4	<0.05	<0.5	5	3.1	5	CIEH/LQM S4UL	d = doing term expsoure provided for illustration only)
WS3	0.4	CMF (clay)	6.6	15	<1	42	24	<1	<3	31	16	87	55	*		 	į		**************************************						- S4UL	LQM/CIEH published Suitable for use levels (2015)
WS4	0.25	made ground (gravel)	7.9	17	<1	31	46	<1	<3	27	23	100	55		CHR	0.4	<0.02	<1	0.4	<0.05	<0.5	1	1.5	3	1	Based on Soil Organic Matter of 1%
WS4	0.45	CMF (clay)	7.7	18	<1	47	33	<1	<3	46	27	110	19		·····		·····								DEFRA	▲= C4SL (2014)
WS5	0.1	topsoil (clay)	5.2	15	<1	38	110	<1	<3	27	18	100	24	<u>.</u>			{								-	(13) = Results have been blank corrected
WS5	0.25	made ground (clay)	5.9	15	<1	40	100	<1	<3	28	15	93	24			<0.2	<0.02	<1	<0.3			<1	0.8	3		ND = None Detected
WS6	0.1	topsoil (clay)	5.5	16	<1	42	60	<1	<3	31	21	120	22				[-	CHR = Chrysofile loose fibres detected
WS6	0.5	CMF (clay)	6.6	13	<1	58	22	<1	<3	33	21	95	18				{	1							~	
WS7	0.15	topsoil (clay)	5.2	16	<1	43	51	<1	<3	37	20	120	19	-											1	
WS7	0.6	CMF (clay)	4.9	15	<1	62	17		<3	30	22	86		0.5		<0.2	<0.02	<1	< 0.3	<0.05		<1	0.6	3		
WS8	0.1	topsoil (clay)	5.4	15	<1	40	52	<1	<3	29	18	110	23				{		-						1	
WS8	0.3	CMF (clay)	5.5	11	<1	55	17	<1	<3	34	20	96	16				{									
WS9	0.2	topsoil (clay)	5.5	17	<1	46	54	<1	<3	33	24	110	22			<0.2	<0.02	<1	<0.3	<0.05	<0.5	<1	0.6	<2		
WS9	0.5	CMF (clay)	5.7	14	<1	44	26	<1	<3	31	17	85	14	1.30	<u>.</u>		<u> </u>	<u>.</u>								
WS10	0.05	topsoil (clay)	5.6	21	<1	52	53	<1	<3	28	77	100	24				<u> </u>									
WS10	0.2	CMF (clay)	6.8	38	<1	66	26	<1	<3	33		100	20	<u>.</u>			<u>.</u>		<u>.</u>							
WS11	0.1	topsoil (clay)	6.9	19	<1	47	35	<1	<3	28	21	110	20	<u>.</u>			L									
WS11	0.5	CMF (clay)	7.0	22	<1	46	23	<1	<3	29	19	140	16	<u>.</u>			<u>i</u>		<u>i</u>							
TIER 1: GE	ENERIC AS	SSESSMENT CRITERIA	<u> </u>		<u> </u>					<u> </u>	<u> </u>			<u>.</u>												
S4UL (Res	sidential wi	ith plant uptake)		37	11	910	200 🜢	40	250	180	2.400	3,700		ļ	1		Ì									
S4UL (Res	sidential wi	ithout plant uptake)	_	40	85	910	310 🜢		430	180	7,100	40,000		<u>;</u>	1		l	1								
S4UL (Allo	tments)		l	43	1.9	18,000			88	230		620			<u>.</u>		{	1	1	1						
S4UL (Con	nmercial)			640	190	8,600	2330 🜢	1,100	12,000	980	68,000	730,000			<u>.</u>		Ì									
S4UL (Pub	olic Open S	Space - Residential)	l	79	120	1,500	630 🔶		1,100	230		81,000			<u>.</u>		{	1	1	1						
		Space - Park)		170			1300 🌢		1,800	3,400	44,000	170,000					ļ		-							
TIER 2: SI	TE SPECIF	FIC								}							{		1	1						
(CIEH Stati	stical Calc	imit [on true mean concentration, u] culator)	Ι	22.6																						
Site-Specifi homegrow	fic Assessm	nent Criteria (SSAC's) residential with		36.5		}	1			1							{		1	1				:		
nomegrow	m produce	,	1	I		\$	WFD "Wat	er Framew	ork Directiv	e Standard	s & Classifica	ation (Englan	d & Wales)	: 2015 (Gr	undwater)	7.5	3.75	37.5	7.5	0.75	75	15	1500	:	1	
	•••••											ngland & Wal					0.08							12.3		
												Directive) (Er				50	-80.0	4.7		0.07		20		8-125	-	
							~~~~~	~~~~~	~~~~~	·····	ards "The Wa				~~~~~	10	0.25 5	50		1	10	20	2000	5000	1	

#### SUMMARY OF POLYAROMATIC HYDROCARBON (PAH) AND INSECTICIDES TESTING RESULTS

<u></u>				77412 111		520 120		00210																																
			1								DROC			(ma/ka)						1						(							0.000			DOUG			<b>D</b> (	
	Ê			1	:	ş	2	POLI			IDKUC/		э (РАП) -	(mg/kg)	:	3		-	;		URG	ANUCH	LURINE	INSECT	ICIDES	(mg/kg)		2	ç	:	5	r	URGA	NOPH	OSPHO	RUUS	INSEC	ICIDES	<b>5</b> (mg/кg	
Sample Ref	Sample Depth (	Sample of	ТОТАL РАН	Naphfhalene	Acenaphthylene	Acenaphthene	Fluorene	Phenanthrene	Anthracene	Fluoranthene	Pyrene	Benzo(a)Arthracene	Chrysene	Benzo(b)Fluorarthene	Benzo(k)Fluoranthene	Benzo(a)Pyrene	Indero(1,2,3)perylene	Dibenzo(ah)Anthracene	Benzo(ghi)Perylene	Hexachilorocyclohexane	Hexachlordbenzene	Heptachlor	Aldrin	Heptachlor epoxide	Chlordane	Endosulphan	DOE	Dieldrin	Endin	QQQ	DOT	Dichlorvos	Mevinphos	Dimethoate	Diazinon	Pirimiphos methyl	Malathion	Fenitrothion	Parathion	Azinphos methyl
WS1	0.3	made ground (clay)	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		<0.1	<0.1				}						[		]				]	{				
WS2	0.3	CMF (clay)				}														<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	(162,131) <0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01	<0.01
WS4	0.45	CMF (clay)	5.1	<0.1	<0.1	<0.1	<0.1	0.6	0.2	1.0	0.9	0.4	0.4	0.4	0.3	0.3	0.2	<0.1	0.2		1	1	1	1												<u> </u>				
WS6	0.5	CMF (clay)	<0.1		<0.1	<0.1	<0.1	<0.1		<0.1	<0.1	<0.1	<0.1		<0.1	<0.1		<0.1					<u> </u>						·····		1	<b> </b>				{		1		
WS8	0.1	topsoil (clay)				}	1	}	1						1		1	1				<0.01	5	÷	1	<0.01		<0.01	<0.01	i .	(162,131) <0.01		<0.01	÷	<0.01	5	<0.01	5	<0.01	
WS10	0.2	CMF (clay)	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1		1	******	1		******				<u> </u>	•••••		h		******	1	<u> </u>	•••••	ţ	•••••	
WS11	0.1	topsoil (clay)							<u>.</u>							1				<0.01		<0.01	2	<0.01		•		5	<0.01		(162,131) <0.01		<0.01		<0.01	(	<0.01	<0.01	<0.01	<0.01
WS11	0.5	CMF (clay)	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1			<0.1				<0.1				\$													}		<u>}</u>		
TIER 1:	GENERIC A	SSESSMENT CRITERIA				[	}	[									1		-				}						[							{				
S4UL (R	esidential w	th plant uptake)		2.3	170	210	170	95	2,400	280	620	7.2	15	2.6	77	2.2 (5	) 27	0.24	320	<u> </u>	1.8	;	5.7					0.97				0.032	<u> </u>			}		<u> </u>		
S4UL (R	esidential w	thout plant uptake)		2.3	2,900	3,000	2,800	1,300	31,000	1,500	3,700	11	30	3.9	110	3.2 (5.3	•) 45	0.31	360		4.1		7.3					7.0	[			6.4				{		{		
S4UL (A	lotments)			4.1	28	34	27	15	380	52	110	2.9	4.1	0.99	37	0.97 (5.7	<b>◆</b> ) 9.5	0.17	290		0.47	<u> </u>	3.2		<u> </u>			0.17			]	0.0049			{	}	<u> </u>	<u>}</u>	<u> </u>	
	ommercial)			al a service a servic		an a	ورور ورور ورور ورور ورور ورور ورور ورو	deren and the second		Junior	54,000		ann an start an an start an an start an an start an		an a	35 (76	) 500	3.50	3,900		110		170					170			<u> </u>	140				<u> </u>		<u>.</u>		
i	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	pace - Residential)			÷	15,000	4	farman		ý	7,400			7.1		Annin	) 82	~			16	ļ	18	Ļ	ļ			8	ļ	ļ	ļ	16		ļ	ļ	Į	ļ	<b>}</b>	ļ	
		pace - Park)		1,200	29,000	29,000	20,000	6,200	150,000	6,300	15,000	49	93	13	370	11 (21	) 150	1.1	1,400		30		30	-				30	<u> </u>		ļ	26	<u> </u>	<u> </u>	<u> </u>	ļ	-	<u>i</u>	-	
	SITE SPECIF			ļ		<u> </u>	ļ	ļ	ļ	}													ļ		ļ				<u> </u>		ļ				<u></u>		ļ	<u>}</u>	ļ	
(CIEH St	atistical Calc						[		<u> </u>						<u>.</u>										<u> </u>										<u> </u>	<u> </u>		<u> </u>		
	cific Assessr wn produce	nent Criteria (SSAC's) residential with				1																	}						{											

uideline in brackets based on health effects following



Concept Life Sciences is a trading name of Concept Life Sciences Analytical & Development Services Limited registered in England and Wales (No 2514788)

### **Concept Life Sciences**

### **Certificate of Analysis**

Hadfield House Hadfield Street Combrook Manchester M16 9FE Tel : 0161 874 2400 Fax : 0161 874 2468

Report Number: 757007-1

Date of Report: 17-Aug-2018

Customer: Wilson Associates (Consulting) Limited 36 Brunswick Road Gloucester GL1 1JJ

Customer Contact: Mr Charlie Morton

Customer Job Reference: 4360/2 Customer Purchase Order: 4360/2/CM Customer Site Reference: Cheltenham Date Job Received at Concept: 03-Aug-2018 Date Analysis Started: 06-Aug-2018 Date Analysis Completed: 17-Aug-2018

The results reported relate to samples received in the laboratory and may not be representative of a whole batch.

Opinions and interpretations expressed herein are outside the scope of UKAS accreditation This report should not be reproduced except in full without the written approval of the laboratory

Tests covered by this certificate were conducted in accordance with Concept Life Sciences SOPs All results have been reviewed in accordance with Section 25 of the Concept Life Sciences, Analytical Services Quality Manual







Report checked and authorised by : Aleksandra Pacula Senior Customer Service Advisor Issued by : Aleksandra Pacula Senior Customer Service Advisor

oulo

Page 1 of 12 757007-1

#### Concept Reference: 757007 Project Site: Cheltenham Customer Reference: 4360/2 Soil Analysed as Soil MCERTS Preparation **Concept Reference** 757007 001 757007 002 757007 006 Customer Sample Reference WS1 WS1 Top Depth 0.10 0.30 Date Sampled 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018

			1	Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
Moisture @105C	T162	AR	0.1	%	23	18	16	20	27
Retained on 10mm sieve	T2	M40	0.1	%	<0.1	<0.1	<0.1	<0.1	<0.1

757007 007

WS2

0.50

WS2

0.30

757007 008

WS3

0.15

Concept Reference: 757007 Project Site: Cheltenham Customer Reference: 4360/2 Soil Analysed as Soil MCERTS Preparation Concept Reference 757007 009 757007 010 757007 011 757007 012 757007 013 WS3 WS4 WS5 WS5 WS4 **Customer Sample Reference** Top Depth 0.40 0.25 0.45 0.10 0.25 Date Sampled 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018 Matrix Class Clay Clay Clay Clay Clay Test Sample Determinand Method LOD Units T162 0.1 % 55 55 Moisture @105C AR 19 24 24 Retained on 10mm sieve T2 M40 0.1 <0.1 % <0.1 < 0.1 < 0.1 <0.1

Concept Refe	erence:	757007							
Proje	ct Site:	Cheltenham	n						
Customer Refe	erence:	4360/2							
Soil		Analysed as	s Soil						
MCERTS Preparation									
			Conce	ot Reference	757007 017	757007 018	757007 019	757007 020	757007 021
		Custon	ner Samp	le Reference	WS6	WS6	WS7	WS7	WS8
				Top Depth	0.10	0.50	0.15	0.60	0.10
			D	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018	31-JUL-201
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
Moisture @105C	sture @105C T162 AR 0.1 %		%	22	18	19	19	23	
Retained on 10mm sieve	T2	M40	0.1	%	<0.1	<0.1	<0.1	<0.1	<0.1

Concept Re	ference:	757007							
Pro	ject Site:	Cheltenhan	n						
Customer Re	ference:	4360/2							
Soil		Analysed a	s Soil						
MCERTS Preparation									
			Conce	ot Reference	757007 022	757007 026	757007 027	757007 031	757007 032
		Custor	ner Sampl	le Reference	WS8	WS9	WS9	WS10	WS10
				Top Depth	0.30	0.20	0.50	0.05	0.20
			D	ate Sampled	31-JUL-2018	31-JUL-2018	31-JUL-2018	30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
Moisture @105C	T162	AR	0.1	%	16	22	14	24	20
Retained on 10mm sieve	T2	M40	0.1	%	<0.1	<0.1	<0.1	<0.1	<0.1

Soil Analysed as Soil MCERTS Preparation Concept Reference 757007 033 757007 034 WS11 WS11 **Customer Sample Reference** Top Depth 0.10 0.50 Date Sampled 30-JUL-2018 30-JUL-2018 Clay Matrix Class Clay Test Sample Determinand Method LOD Units Moisture @105C T162 AR 0.1 % 20 16 M40 0.1 <0.1 Retained on 10mm sieve Т2 % <0.1

> Concept Reference: 757007 Project Site: Cheltenham

Soil

Customer Reference: 4360/2

Analysed as Soil

User Metale (0)		/ maryood i							
Heavy Metals(9)									
			Conce	ept Reference	757007 001	757007 002	757007 006	757007 007	757007 008
		Custom	ner Sam	ple Reference	WS1	WS1	WS2	WS2	WS3
				Top Depth	0.10	0.30	0.30	0.50	0.15
			1	Date Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
Arsenic	T6	M40	2	mg/kg	22	21	16	15	16
Cadmium	Т6	M40	1	mg/kg	1	<1	<1	<1	<1
Chromium	Т6	M40	1	mg/kg	35	43	42	53	37
Copper	Т6	M40	1	mg/kg	41	23	21	22	23
Lead	Т6	M40	1	mg/kg	190	79	27	32	110
Mercury	T6	M40	1	mg/kg	<1	<1	<1	<1	<1
Nickel	Т6	M40	1	mg/kg	32	31	35	33	26
Selenium	T6	M40	3	mg/kg	<3	<3	<3	<3	<3
Zinc	Т6	M40	1	mg/kg	190	100	100	94	130

Concept Reference: 757007 Project Site: Cheltenham

Customer Reference: 4360/2

Soil

#### Analysed as Soil

Heavy Metals(9)

			Conce	ept Reference	757007 009	757007 010	757007 011	757007 012	757007 013
		Custon	ner Samp	ole Reference	WS3	WS4	WS4	WS5	WS5
				Top Depth	0.40	0.25	0.45	0.10	0.25
			[	Date Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
Arsenic	Т6	M40	2	mg/kg	15	17	18	15	15
Cadmium	T6	M40	1	mg/kg	<1	<1	<1	<1	<1
Chromium	Т6	M40	1	mg/kg	42	31	47	38	40
Copper	Т6	M40	1	mg/kg	16	23	27	18	15
Lead	Т6	M40	1	mg/kg	24	46	33	110	100
Mercury	Т6	M40	1	mg/kg	<1	<1	<1	<1	<1
Nickel	T6	M40	1	mg/kg	31	27	46	27	28
Selenium	Т6	M40	3	mg/kg	<3	<3	<3	<3	<3
Zinc	Т6	M40	1	mg/kg	87	100	110	100	93

Analysed as Soil

Soil

Heavy Metals(9)									
			Concep	t Reference	757007 017	757007 018	757007 019	757007 020	757007 021
		Custon	ner Sampl	e Reference	WS6	WS6	WS7	WS7	WS8
				Top Depth	0.10	0.50	0.15	0.60	0.10
			Da	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018	31-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
Arsenic	T6	M40	2	mg/kg	16	13	16	15	15
Cadmium	T6	M40	1	mg/kg	<1	<1	<1	<1	<1
Chromium	T6	M40	1	mg/kg	42	58	43	62	40
Copper	T6	M40	1	mg/kg	21	21	20	22	18
Lead	T6	M40	1	mg/kg	60	22	51	17	52
Mercury	T6	M40	1	mg/kg	<1	<1	<1	<1	<1
Nickel	T6	M40	1	mg/kg	31	33	37	30	29
Selenium	T6	M40	3	mg/kg	<3	<3	<3	<3	<3
Zinc	T6	M40	1	mg/kg	120	95	120	86	110

Concept Reference: 757007 Project Site: Cheltenham Customer Reference: 4360/2

Soil		Analysed	as Soil				
Heavy Metals(9)							
		_	Conce	ot Reference	757007 022	757007 026	757007 027
		Custon	ner Sampl	le Reference	WS8	WS9	WS9
			1.4	Top Depth	0.30	0.20	0.50
			D	ate Sampled	31-JUL-2018	31-JUL-2018	31-JUL-2018
				Matrix Class	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units			
Arsenic	Т6	M40	2	mg/kg	-11	17	14
Cadmium	Т6	M40	1	mg/kg	<1	<1	<1
Chromium	T6	M40	1	mg/kg	55	46	44

Determinand	Method	Sample	LOD	Units					-
Arsenic	Т6	M40	2	mg/kg	11	17	14	21	38
Cadmium	Т6	M40	1	mg/kg	<1	<1	<1	<1	<1
Chromium	T6	M40	1	mg/kg	55	46	44	52	66
Copper	Т6	M40	1	mg/kg	20	24	17	77	28
Lead	Т6	M40	1	mg/kg	17	54	26	53	26
Mercury	T6	M40	1	mg/kg	<1	<1	<1	<1	<1
Nickel	Т6	M40	1	mg/kg	34	33	31	28	33
Selenium	T6	M40	3	mg/kg	<3	<3	<3	<3	<3
Zinc	Т6	M40	1	mg/kg	96	110	85	100	100

757007 031 757007 032

30-JUL-2018 30-JUL-2018

WS10

0.20

Clay

WS10

0.05

Clay

Concept	Reference:	757007				
I	Project Site:	Cheltenha	am			
Custome	Reference:	4360/2				- 0.0
Soil		Analysed	as Soil			
Heavy Metals(9)						
			Conce	pt Reference	757007 033	757007 034
		Custor	ner Samp	le Reference	WS11	WS11
				Top Depth	0.10	0.50
				ate Sampled	30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay
Determinand	Method	Test Sample	LOD	Units		
Arsenic	Т6	M40	2	mg/kg	19	22
Cadmium	Т6	M40	1	mg/kg	<1	<1
Chromium	Т6	M40	1	mg/kg	47	46
Copper	Т6	M40	1	mg/kg	21	19
Lead	Т6	M40	1	mg/kg	35	23
Mercury	T6	M40	1	mg/kg	<1	<1
Nickel	Т6	M40	1	mg/kg	28	29
Selenium	Т6	M40	3	mg/kg	<3	<3
Zinc	Т6	M40	1	mg/kg	110	140

Analysed as Soil

Analysed as Soil

Soil

Wilson Sulphate Suite

			ot Reference	757007 003	757007 004	757007 005	757007 014	757007 015	
	WS1	WS1	WS1	WS5	WS5				
	Top Depth							1.00	2.00
	Date Sample							30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
pН	T7	A40			6.8	7.9	7.7	6.8	7.8
(Water soluble) SO4 as SO3	T251	A40	0.01	g/l	0.04	0.70	1.9	0.02	0.04
(Water Soluble) SO4 expressed as SO4	T242	A40	0.05	g/l	<0.05	0.84	2.2	<0.05	<0.05
(Acid Soluble) SO4	T192	A40	0.01	%	0.04	0.19	4.9	0.01	0.03
Sulphur (total)	Т6	A40	0.01	%	0.02	0.07	1.7	0.01	0.01
(Total Potential) SO4(Total) Expressed as SO4	T403	A40	0.03	%	0.06	0.21	5.1	0.03	0.03
(Oxidisable) Sulphide Expressed as SO4	T194	A40	0.03	%	<0.03	<0.03	0.20	<0.03	<0.03

Concept Reference: 757007 Project Site: Cheltenham

Customer Reference: 4360/2

Soil

Wilson Sulphate Suite

			Concep	t Reference	757007 016	757007 023	757007 024	757007 025	757007 028
		Custon	ner Sampl	e Reference	WS5	WS8	WS8	WS8	WS9
				Top Depth	3.00	1.30	2.30	3.30	0.70
100			Da	ate Sampled	30-JUL-2018	31-JUL-2018	31-JUL-2018	31-JUL-2018	31-JUL-2018
	141.0			Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units		10.00			
pH	T7	A40	1.2		7.5	6.9	7.8	7.4	6.0
(Water soluble) SO4 as SO3	T251	A40	0.01	g/l	0.06	0.01	0.02	0.02	0.01
(Water Soluble) SO4 expressed as SO4	T242	A40	0.05	g/l	0.07	<0.05	<0.05	<0.05	<0.05
(Acid Soluble) SO4	T192	A40	0.01	%	0.03	<0.01	0.03	0.03	0.04
Sulphur (total)	T6	A40	0.01	%	0.02	<0.01	0.01	0.05	0.02
(Total Potential) SO4(Total) Expressed as SO4	T403	A40	0.03	%	0.06	<0.03	0.03	0.15	0.06
(Oxidisable) Sulphide Expressed as SO4	T194	A40	0.03	%	0.03	< 0.03	< 0.03	0.12	< 0.03

Concept Reference: 75700	7					
Project Site: Chelte	enham					
Customer Reference: 4360/2	2					
Soil Analys Wilson Sulphate Suite	sed as Soil					
				ot Reference	757007 029	757007 030
		Custon	ner Samp	e Reference	WS9	WS9
				Top Depth	1.70	2.70
			D	ate Sampled	31-JUL-2018	31-JUL-2018
				Matrix Class	Clay	Clay
Determinand	Method	Test Sample	LOD	Units		
рН	T7	A40			5.8	7.4
(Water soluble) SO4 as SO3	T251	A40	0.01	g/l	<0.01	<0.01
(Water Soluble) SO4 expressed as SO4	T242	A40	0.05	g/l	<0.05	<0.05
(Acid Soluble) SO4	T192	A40	0.01	%	0.01	0.01
Sulphur (total)	Т6	A40	0.01	%	<0.01	<0.01
(Total Potential) SO4(Total) Expressed as S	iO4 T403	A40	0.03	%	<0.03	<0.03
(Oxidisable) Sulphide Expressed as SO4	T194	A40	0.03	%	<0.03	<0.03

-	,			
rence:	757007			
t Site:	Cheltenha	am		
rence:	4360/2			
	Analysed	as Soil		
		Conce	pt Reference	757007 010
	Custon	ner Sampl	le Reference	WS4
			Top Depth	0.25
		D	ate Sampled	30-JUL-2018
			Matrix Class	Clay
ethod	Test Sample	LOD	Units	
Г27	A40			Chrysotile Loose Fibres Detected
	t Site: rence:	rence: 4360/2 Analysed Custon thod Test Sample	t Site: Cheltenham rence: 4360/2 Analysed as Soil Conce Customer Samp D thod Test Sample LOD	t Site: Cheltenham rence: 4360/2 Analysed as Soil Concept Reference Customer Sample Reference Top Depth Date Sampled Matrix Class

Concept Reference: 757007 Project Site: Cheltenham Customer Reference: 4360/2 Soil Analysed as Soil Miscellaneous Concept Reference 757007 001 757007 002 757007 006 757007 007 757007 008 WS1 WS1 WS2 WS2 WS3 Customer Sample Reference Top Depth 0.10 0.30 0.30 0.50 0.15 Date Sampled 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018 Matrix Class Clay Clay Clay Clay Clay Test Sample Determinand Method LOD Units Τ7 pН A40 5.9 6.6 6.0 6.3 5.9 Soil Organic Matter T287 0.1 1.0 A40 %

Concept Reference: 757007 Project Site: Cheltenham Customer Reference: 4360/2 Soil Analysed as Soil Miscellaneous 757007 009 757007 010 757007 011 757007 012 757007 013 **Concept Reference** WS3 WS4 **Customer Sample Reference** WS4 WS5 WS5 Top Depth 0.40 0.25 0.45 0.10 0.25 Date Sampled 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018 30-JUL-2018 Matrix Class Clay Clay Clay Clay Clay Test Sample Determinand Method LOD Units pН Τ7 A40 6.6 7.9 7.7 5.2 5.9

Concept R	Reference:	757007							
Pr	oject Site:	Cheltenha	am						
Customer R	Reference:	4360/2							
Soil		Analysed	as Soil						
Miscellaneous									
			Concep	t Reference	757007 017	757007 018	757007 019	757007 020	757007 021
		Custor	ner Sampl	e Reference	WS6	WS6	WS7	WS7	WS8
				Top Depth	0.10	0.50	0.15	0.60	0.10
			D	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018	31-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
pН	T7	A40			5.5	6.6	5.2	4.9	5.4
Soil Organic Matter	T287	A40	0.1	%	-	-	-	0.5	-

Soil		Analysed	as Soil						
Miscellaneous									
			Conce	ot Reference	757007 022	757007 026	757007 027	757007 031	757007 032
		Custon	ner Sampl	le Reference	WS8	WS9	WS9	WS10	WS10
				Top Depth	0.30	0.20	0.50	0.05	0.20
			D	ate Sampled	31-JUL-2018	31-JUL-2018	31-JUL-2018	30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
pН	T7	A40			5.5	5.5	5.7	5.6	6.8
Soil Organic Matter	T287	A40	0.1	%	-	-	1.3	-	-

Г						
Concept R	eference:	757007				
Pro	oject Site:	Cheltenha	am			
Customer R	eference:	4360/2				
Soil		Analysed	as Soil			
Miscellaneous						
			Conce	pt Reference	757007 033	757007 034
		Custon	ner Sam	ble Reference	WS11	WS11
				Top Depth	0.10	0.50
			[	Date Sampled	30-JUL-2018	30-JUL-2018
			_	Matrix Class	Clay	Clay
Determinand	Method	Test Sample	LOD	Units		
pН	T7	A40			6.9	7.0

Concept Reference: 757007 Project Site: Cheltenham

Customer Reference: 4360/2

Soil

Analysed as Soil PAH US EPA 16 (B and K split)

					A Contraction of the second				
			Concep	ot Reference	757007 002	757007 011	757007 018	757007 032	757007 034
		Custon	ner Sampl	e Reference	WS1	WS4	WS6	WS10	WS11
				Top Depth	0.30	0.45	0.50	0.20	0.50
			D	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
Naphthalene	T207	M105	0.1	mg/kg	<0.1	<0.1	<0.1	<0.1	<0.1
Acenaphthylene	T207	M105	0.1	mg/kg	<0.1	<0.1	<0.1	<0.1	<0.1
Acenaphthene	T207	M105	0.1	mg/kg	<0.1	<0.1	<0.1	<0.1	<0.1
Fluorene	T207	M105	0.1	mg/kg	<0.1	<0.1	<0.1	<0.1	<0.1
Phenanthrene	T207	M105	0.1	mg/kg	<0.1	0.6	<0.1	<0.1	<0.1
Anthracene	T207	M105	0.1	mg/kg	<0.1	0.2	<0.1	<0.1	<0.1
Fluoranthene	T207	M105	0.1	mg/kg	<0.1	1.0	<0.1	<0.1	<0.1
Pyrene	T207	M105	0.1	mg/kg	<0.1	0.9	<0.1	<0.1	<0.1
Benzo(a)Anthracene	T207	M105	0.1	mg/kg	<0.1	0.4	<0.1	<0.1	<0.1
Chrysene	T207	M105	0.1	mg/kg	<0.1	0.4	<0.1	<0.1	<0.1
Benzo(b)fluoranthene	T207	M105	0.1	mg/kg	<0.1	0.4	<0.1	<0.1	<0.1
Benzo(k)fluoranthene	T207	M105	0.1	mg/kg	<0.1	0.3	<0.1	<0.1	<0.1
Benzo(a)Pyrene	T207	M105	0.1	mg/kg	<0.1	0.3	<0.1	<0.1	<0.1
Indeno(123-cd)Pyrene	T207	M105	0.1	mg/kg	<0.1	0.2	<0.1	<0.1	<0.1
Dibenzo(ah)Anthracene	T207	M105	0.1	mg/kg	<0.1	<0.1	<0.1	<0.1	<0.1
Benzo(ghi)Perylene	T207	M105	0.1	mg/kg	<0.1	0.2	<0.1	<0.1	<0.1
PAH(total)	T207	M105	0.1	mg/kg	<0.1	5.1	<0.1	<0.1	<0.1

Analysed as Soil

Soil

Organochlorine insecticides

Organochlorine insecticides							
			Conce	ot Reference	757007 006	757007 021	757007 033
		Custon	ner Samp	le Reference	WS2	WS8	WS11
				Top Depth	0.30	0.10	0.10
			D	ate Sampled	30-JUL-2018	31-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units			
Hexachlorocyclohexane (sum of alpha, beta and gamma)	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Hexachlorobenzene	T1	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Heptachlor	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Aldrin	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Heptachlor epoxide	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Chlordane	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Endosulphan	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
DDE	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Dieldrin	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Endrin	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
DDD	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
DDT	T16	AR	0.01	mg/kg	(162,131) <0.02	(131,162) <0.02	(131,162) <0.02

Concep	t Reference:	757007			1.00	1.1.1.1.1	
1	Project Site:	Cheltenha	ım				
Custome	r Reference:	4360/2					
Soil		Analysed	as Soil				
Organophosphorous	insecticides						
		1	Conce	ot Reference	757007 006	757007 021	757007 033
		Custon	ner Sampl	e Reference	WS2	WS8	WS11
			1000	Top Depth	0.30	0.10	0.10
		100	D	ate Sampled	30-JUL-2018	31-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units			
Dichlorvos	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Mevinphos	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Dimethoate	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Diazinon	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Pirimiphos methyl	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Malathion	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Fenitrothion	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Parathion	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01
Azinphos methyl	T16	AR	0.01	mg/kg	<0.01	<0.01	<0.01

#### Concept Reference: 757007 Project Site: Cheltenham Customer Reference: 4360/2 Soil Analysed as Soil BS 3882:2015 **Concept Reference** 757007 035 757007 036 757007 037 West Topsoil **Customer Sample Reference** Cent Topsoil East Topsoil Date Sampled 30-JUL-2018 31-JUL-2018 30-JUL-2018 Clay Matrix Class Clay Clay Test Sample Method LOD Determinand Units T85 Ratio 10:1 Ratio 10:1 Ratio 13:1 Carbon / Nitrogen ratio AR T22 AR Carbonate 0.1 % 0.6 0.6 0.5 Clay Content T2 AR 1.0 % 36 41 39 Dry density T85 AR 0.1 0.5 0.9 0.6 g/cm3 Electrical Conductivity Τ7 A40 10 µS/cm 2100 1900 2100 LOI (OM) (125-440)C T873 A40 19.1 17.7 % 22.0 Mg (Extractable BS 3882) T272 A40 10 95 200 22 mg/l Nitrogen (Total) T837 AR 100 mg/kg 6100 2400 4900 pН T7 A40 5.5 6.3 5.7 Extractable P T392 AR 10 mg/l 47 12 23 K (Extractable BS 3882) T272 A40 10 mg/l 140 110 18 Sand Content T2 AR 1.0 % 19 9.0 11 Silt Content 50 T2 AR 1.0 % 45 50

Concept Reference: 757007 Project Site: Cheltenham Customer Reference: 4360/2

T21

T161

A40

AR

0.1

0.5

%

%

4.0

<0.5

2.0

<0.5

5.7

<0.5

Total Organic Carbon

Visible Contaminants

Soil % Stones		Analysed	as Soil				
		3	Concep	ot Reference	757007 035	757007 036	757007 037
		Custor	ner Sampl	e Reference	West Topsoil	Cent Topsoil	East Topsoil
			Da	ate Sampled	30-JUL-2018	31-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units	1400		
Retained on 20mm	T2	AR	0.1	%	<0.1	<0.1	<0.1
Retained on 2mm	T2	A40	0.1	%	4.8	3.8	5.2
Retained on 50mm	T2	AR	0.1	%	<0.1	<0.1	<0.1

Concept F	Reference:	757007				1.0	
Pr	oject Site:	Cheltenha	am				
Customer F	Reference:	4360/2					
Soil Phytotoxic Contaminan	ts	Analysed	as Soil				7
			Conce	pt Reference	757007 035	757007 036	757007 037
		Custon	ner Samp	ole Reference	West Topsoil	Cent Topsoil	East Topsoil
			0	Date Sampled	30-JUL-2018	31-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units			
Copper	T312	A40	1	mg/kg	22	16	16
Nickel	T312	A40	1	mg/kg	24	25	23
Zinc	T312	A40	1	mg/kg	110	89	100

Concept Re	eference:	757007							
Pro	ject Site:	Cheltenha	ım						
Customer Re	- eference:	4360/2							
Leachate Heavy Metals(9)		Analysed	as Water						
			Conce	pt Reference	757007 008	757007 010	757007 013	757007 020	757007 026
		Custon	ner Samp	le Reference	WS3	WS4	WS5	WS7	WS9
				Top Depth	0.15	0.25	0.25	0.60	0.20
			D	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018	30-JUL-2018	31-JUL-2018
				Matrix Class	Clay	Clay	Clay	Clay	Clay
Determinand	Method	Test Sample	LOD	Units					
As (Dissolved)	T281	10:1	0.2	µg/l	0.3	0.4	<0.2	<0.2	<0.2
Cd (Dissolved)	T281	10:1	0.02	µg/l	<0.02	<0.02	<0.02	<0.02	<0.02
Cr (Dissolved)	T281	10:1	1	µg/l	9	<1	<1	<1	<1
Cu (Dissolved)	T281	10:1	0.5	µg/l	3.1	1.5	0.8	0.6	0.6
Pb (Dissolved)	T281	10:1	0.3	µg/l	0.4	0.4	<0.3	<0.3	<0.3
Hg (Dissolved)	T281	10:1	0.05	µg/l	<0.05	<0.05	<0.05	<0.05	<0.05
Ni (Dissolved)	T281	10:1	1	µg/l	5	1	<1	<1	<1
Se (Dissolved)	T281	10:1	0.5	µg/l	<0.5	<0.5	<0.5	<0.5	<0.5
Zn (Dissolved)	T281	10:1	2	µg/l	5	3	3	3	<2

### Index to symbols used in 757007-1

Value	Description
A40	Assisted dried < 40C
M40	Analysis conducted on sample assisted dried at no more than 40C. Results are reported on a dry weight basis.
AR	As Received
M105	Analysis conducted on an "as received" aliquot. Results are reported on a dry weight basis where moisture content was determined by assisted drying of sample at 105C
10:1	Leachate
162	LOD determined by matrix spike recovery
131	Result is outside of the scope of accreditation due to a QC Failure
S	Analysis was subcontracted
М	Analysis is MCERTS accredited
U	Analysis is UKAS accredited
Ν	Analysis is not UKAS accredited

#### Notes

Asbestos was subcontracted to REC Asbestos. Nitrogen and Sand/Silt/Clay content were subcontracted to NRM.

#### **Method Index**

Value	Description
T7	Probe
T272	ICP/OES (Ammonium Nitrate)
T6	ICP/OES
T161	Visual
T242	2:1 Extraction/ICP/OES (TRL 447 T1)
T287	Calc TOC/0.58
T312	ICP-OES (Nitric Acid Extraction)
T1	GC/MS (HR)
T194	Calc (TRL 447 T 4.11)
T403	Calc (TRL 447 T4.13 ICP/OES)
T27	PLM
T251	2:1 Extraction/ICP/OES
T192	HCI Extraction/ICP/OES (TRL 447 T2)
T837	CSOP Nut007 (Dumas)
T873	Grav (4 Dec) (Dry 125 C)(Ign 440 C)
T2	Grav
T21	OX/IR
T22	Titration
T162	Grav (1 Dec) (105 C)
T207	GC/MS (MCERTS)

T281	ICP/MS (Filtered)
T85	Calc
T392	ICP/OES (Sodium Hydrogen Carbonate Extract)
T16	GC/MS

### **Accreditation Summary**

Determinand	Method	Test	LOD	Units	Symbol	Concept References
		Sample	LOD	Units	-	
Carbon / Nitrogen ratio	T85	AR			N	035-037
Carbonate	T22	AR	0.1	%	N	035-037
Clay Content	T2	AR	1.0	%	SN	035-037
Dry density	T85	AR	0.1	g/cm3	N	035-037
Electrical Conductivity	T7	A40	10	µS/cm	N	035-037
LOI (OM) (125-440)C	T873	A40		%	N	035-037
Mg (Extractable BS 3882)	T272	A40	10	mg/l	N	035-037
Nitrogen (Total)	T837	AR	100	mg/kg	SN	035-037
Extractable P	T392	AR	10	mg/l	N	035-037
K (Extractable BS 3882)	T272	A40	10	mg/l	N	035-037
Sand Content	T2	AR	1.0	%	SN	035-037
Silt Content	T2	AR	1.0	%	SN	035-037
Total Organic Carbon	T21	A40	0.1	%	N	035-037
Visible Contaminants	T161	AR	0.5	%	N	035-037
Retained on 20mm	T2	AR	0.1	%	N	035-037
Retained on 2mm	T2	A40	0.1	%	N	035-037
Retained on 50mm	T2	AR	0.1	%	N	035-037
Copper	T312	A40	1	mg/kg	N	035-037
Nickel	T312	A40 A40	1	mg/kg	N	035-037
Zinc	T312	A40 A40	1		N	035-037
pH	T7	A40 A40	1	mg/kg	M	001-002,006-013,017-022,026-027,031-034
			0.4	0/		
Soil Organic Matter	T287	A40	0.1	%	N	007,020,027
Hexachlorocyclohexane (sum of alpha, beta and gamma)	T16	AR	0.01	mg/kg	U	006,021,033
Hexachlorobenzene	T1	AR	0.01	mg/kg	U	006,021,033
Heptachlor	T16	AR	0.01	mg/kg	U	006,021,033
Aldrin	T16	AR	0.01	mg/kg	U	006,021,033
Heptachlor epoxide	T16	AR	0.01	mg/kg	U	006,021,033
Chlordane	T16	AR	0.01	mg/kg	U	006,021,033
Endosulphan	T16	AR	0.01	mg/kg	U	006,021,033
DDE	T16	AR	0.01	mg/kg	U	006,021,033
Dieldrin	T16	AR	0.01	mg/kg	U	006,021,033
Endrin	T16	AR	0.01	mg/kg	U	006,021,033
DDD	T16	AR	0.01	mg/kg	U	006,021,033
DDT	T16	AR	0.01	mg/kg	U	006,021,033
Naphthalene	T207	M105	0.1	mg/kg	М	002,011,018,032,034
Acenaphthylene	T207	M105	0.1	mg/kg	U	002,011,018,032,034
Acenaphthene	T207	M105	0.1	mg/kg	м	002,011,018,032,034
Fluorene	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Phenanthrene	T207	M105	0.1	mg/kg	м	002,011,018,032,034
Anthracene	T207	M105	0.1	mg/kg	U	002,011,018,032,034
Fluoranthene	T207	M105	0.1		м	002,011,018,032,034
	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Pyrene				mg/kg		
Benzo(a)Anthracene	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Chrysene	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Benzo(b)fluoranthene	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Benzo(k)fluoranthene	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Benzo(a)Pyrene	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Indeno(123-cd)Pyrene	T207	M105	0.1	mg/kg	M	002,011,018,032,034
Dibenzo(ah)Anthracene	T207	M105	0.1	mg/kg	М	002,011,018,032,034
Benzo(ghi)Perylene	T207	M105	0.1	mg/kg	М	002,011,018,032,034
PAH(total)	T207	M105	0.1	mg/kg	U	002,011,018,032,034
Dichlorvos	T16	AR	0.01	mg/kg	U	006,021,033
Mevinphos	T16	AR	0.01	mg/kg	U	006,021,033
Dimethoate	T16	AR	0.01	mg/kg	U	006,021,033
Diazinon	T16	AR	0.01	mg/kg	U	006,021,033
Pirimiphos methyl	T16	AR	0.01	mg/kg	U	006,021,033
	T16	AR	0.01	mg/kg	U	006,021,033
Malathion					U	006,021,033
Malathion Fenitrothion	T16	AR	0.01	l ma/ka		
Fenitrothion	T16 T16	AR AR	0.01	mg/kg mg/kg		
Fenitrothion Parathion	T16	AR	0.01	mg/kg	U	006,021,033
Fenitrothion						

Determinand	Method	Test Sample	LOD	Units	Symbol	Concept References
Cd (Dissolved)	T281	10:1	0.02	µg/l	U	008,010,013,020,026
Cr (Dissolved)	T281	10:1	1	µg/l	U	008,010,013,020,026
Cu (Dissolved)	T281	10:1	0.5	µg/l	U	008,010,013,020,026
Pb (Dissolved)	T281	10:1	0.3	µg/l	U	008,010,013,020,026
Hg (Dissolved)	T281	10:1	0.05	µg/l	U	008,010,013,020,026
Ni (Dissolved)	T281	10:1	1	µg/l	U	008,010,013,020,026
Se (Dissolved)	T281	10:1	0.5	µg/l	U	008,010,013,020,026
Zn (Dissolved)	T281	10:1	2	µg/l	U	008,010,013,020,026
Arsenic	T6	M40	2	mg/kg	М	001-002,006-013,017-022,026-027,031-034
Cadmium	T6	M40	1	mg/kg	м	001-002,006-013,017-022,026-027,031-034
Chromium	T6	M40	1	mg/kg	М	001-002,006-013,017-022,026-027,031-034
Copper	T6	M40	1	mg/kg	м	001-002,006-013,017-022,026-027,031-034
Lead	T6	M40	1	mg/kg	м	001-002,006-013,017-022,026-027,031-034
Mercury	T6	M40	1	mg/kg	М	001-002,006-013,017-022,026-027,031-034
Nickel	T6	M40	1	mg/kg	м	001-002,006-013,017-022,026-027,031-034
Selenium	T6	M40	3	mg/kg	м	001-002,006-013,017-022,026-027,031-034
Zinc	T6	M40	1	mg/kg	М	001-002,006-013,017-022,026-027,031-034
Moisture @105C	T162	AR	0.1	%	N	001-002,006-013,017-022,026-027,031-034
Retained on 10mm sieve	T2	M40	0.1	%	N	001-002,006-013,017-022,026-027,031-034
рН	T7	A40			U	003-005,014-016,023-025,028-030,035-037
(Water soluble) SO4 as SO3	T251	A40	0.01	g/l	N	003-005,014-016,023-025,028-030
(Water Soluble) SO4 expressed as SO4	T242	A40	0.05	g/l	U	003-005,014-016,023-025,028-030
(Acid Soluble) SO4	T192	A40	0.01	%	U	003-005,014-016,023-025,028-030
Sulphur (total)	T6	A40	0.01	%	U	003-005,014-016,023-025,028-030
(Total Potential) SO4(Total) Expressed as SO4	T403	A40	0.03	%	U	003-005,014-016,023-025,028-030
(Oxidisable) Sulphide Expressed as SO4	T194	A40	0.03	%	U	003-005,014-016,023-025,028-030





Job No. 4360/2

# **APPENDIX 3**

TOPSOIL CERTIFICATE OF ANALYSIS (BS3882:2015)



Certificate of	Analysis	
Client:Robert Hitchins LimitedClient Reference:Oakley FarmSuite ID:BS 3882:2015Site Details:Harp Hill, Cheltenham	Date Received: Date Reported:	4360/2 03/08/18 17/08/18 CM
Soil Sample Reference: Western Fields - 0	Composite Sample (WS1 -	- WS3)
Particle Size Distribution*	(UK Classification)	
Clay (<0.002mm) Silt (0.002-0.06mm) Sand (0.06-2.0mm) Textual Class	% % %	36 45 19 ZC ×
	√	
Stone Content (Dry Weight Basis)	r	
Stones 2-20mm Stones 20-50mm Stones >50mm	%w/w %w/w %w/w	4.8     ✓       <0.1
Soil Reaction & Soluble Salts		
pH Value	units µS/cm	5.5 ✓ 2100 ✓
Organic Matter & Nutrient Status		
Organic Matter (LOI) Total Nitrogen Carbon: Nitrogen Ratio Total Organic Carbon Carbonate Extractable Phosphate Extractable Potassium Extractable Magnesium Dry Density	% % % mg/l mg/l g/cm ³	$\begin{array}{c c} 22.0 \times \\ \hline 6100 \\ 10:1 \checkmark \\ 4.0 \\ 0.6 \\ 47 \checkmark \\ 140 \checkmark \\ 95 \checkmark \\ 0.5 \\ \hline$
Phytotoxic Metals'		
Zinc (Zn) Copper (Cu) Nickel (Ni)	mg/kg mg/kg mg/kg	110     ✓       22     ✓       24     ✓
Visibile Contaminants (Dry Weight Basis)		
Total foreign matter > 2mm of which plastics of which sharps	%w/w %w/w %w/w	<0.5 🗸
Soil Description		
Notes:	UK Soil Texture	Classification
<ul> <li>☑ Conforms to BS3882:2015 Multipurpose Grade</li> <li>☑ Fails to conform to BS3882:2015 Multipurpose Grade</li> </ul>	C Clay SC Sandy Clay CL Clay loam	ZC Silty Clay ZCL Silty Clay Loam SZL Sandy Silt Loam
* ADAS pipette ◆ 1:2.5 water extract ◆ CaSO₄ extract ' Total metals ne not evaluated	SL Sandy Loam SCL Sandy Clay Lo LS Loamy Sand	ZL Silt Loam

Sample(s) were analysed at the UKAS accredited laboratory of NRM



Certificate of Analysis								
Client:Robert Hitchins LimitedClient Reference:Oakley FarmSuite ID:BS 3882:2015Site Details:Harp Hill, Cheltenham	Date Received: ( Date Reported:	4360/2 03/08/18 17/08/18 CM						
Soil Sample Reference: Central Fields - Con	mposite Sample (WS4, W	 IS7 - WS8 and WS10						
Particle Size Distribution*	(UK Classification)							
Clay (<0.002mm) Silt (0.002-0.06mm)	% %	41 50 9						
Textual Class	[	ZC ×						
Stone Content (Dry Weight Basis)								
Stones 2-20mm Stones 20-50mm Stones >50mm	%w/w %w/w %w/w	3.8 ✓ <0.1 ✓ <0.1 ✓						
Soil Reaction & Soluble Salts								
pH Value ❖ Electrical Conductivity (CaSO₄) <b>+</b>	units μS/cm	6.3 ✓ 1900 ✓						
Organic Matter & Nutrient Status								
Organic Matter (LOI) Total Nitrogen Carbon: Nitrogen Ratio Total Organic Carbon Carbonate Extractable Phosphate Extractable Potassium Extractable Magnesium	% % % mg/l mg/l mg/l	$ \begin{array}{c cccc} 19.1 & \checkmark \\ 2400 \\ \hline 10:1 & \checkmark \\ 2.0 \\ \hline 0.6 \\ \hline 12 & \times \\ 110 & \times \\ 200 & \checkmark \end{array} $						
Dry Density	g/cm³	0.9						
Phytotoxic Metals'								
Zinc (Zn) Copper (Cu) Nickel (Ni)	mg/kg mg/kg mg/kg	89         ✓           16         ✓           25         ✓						
Visibile Contaminants (Dry Weight Basis)								
Total foreign matter > 2mm of which plastics of which sharps	%w/w %w/w %w/w	<0.5 ✓						
Soil Description								
Notes:	UK Soil Texture	Classification						
<ul> <li>Conforms to BS3882:2015 Multipurpose Grade</li> <li>Fails to conform to BS3882:2015 Multipurpose Grade</li> </ul>	C Clay SC Sandy Clay CL Clay Ioam	ZC Silty Clay ZCL Silty Clay Loam SZL Sandy Silt Loam						
* ADAS pipette ◆ 1:2.5 water extract ◆ CaSO₄ extract ' Total metals	SL Sandy Loam SCL Sandy Clay Lo LS Loamy Sand	ZL Silt Loam oam S Sand						

Sample(s) were analysed at the UKAS accredited laboratory of NRM



Certificate	of Analysis
-------------	-------------

	Certificate o	1 Allalysis	
Client: Client Reference: Suite ID: Site Details:	Robert Hitchins Limited Oakley Farm BS 3882:2015 Harp Hill, Cheltenham	<i>Our Ref: Date Received: Date Reported: Sampled by:</i>	4360/2 03/08/18 17/08/18 CM
Soil Sample Refere	nce: Eastern Fields - C	omposite Sample (WS5	5 - WS7, WS9 and WS11)
Particle Size Distribution*		(UK Classification	n)
Clay (<0.002mm) Silt (0.002-0.06mm) Sand (0.06-2.0mm) Textual Class		% % %	39 50 11 ZC ×
Stone Content (Dry Weight	Basis)		
Stones 2-20mm Stones 20-50mm Stones >50mm		%w/w %w/w %w/w	5.2     ✓       <0.1
Soil Reaction & Soluble Sal	ts		
pH Value	ity (CaSO₄) <b>+</b>	units μS/cm	5.7 × 2100 ×
Organic Matter & Nutrient S	tatus		
Organic Matter (LO Total Nitrogen Carbon: Nitrogen R Total Organic Carbo Carbonate Extractable Phosph Extractable Potassi Extractable Magnes Dry Density	atio n ate um	% % % mg/l mg/l g/cm ³	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$
Phytotoxic Metals'			
Zinc (Zn) Copper (Cu) Nickel (Ni)		mg/kg mg/kg mg/kg	100         ✓           16         23
Visibile Contaminants (Dry	Weight Basis)		
Total foreign matter of which plastics of which sharps	> 2mm	%w/w %w/w %w/w	<0.5
Soil Description			
Notes:		UK Soil Texture	e Classification
☑ Conforms to BS3882:2015 M ☑ Fails to conform to BS3882:2		C Clay SC Sandy Clay	ZC Silty Clay ZCL Silty Clay Loam
* ADAS pipette ◆ 1:2.5 water extract ➡ CaSO₄ extract ' Total metals ne not evaluated		CL Clay loam SL Sandy Loam SCL Sandy Clay LS Loamy Sand	Loam S Sand I
	Sample(s) were analysed at the L	IKAS accredited laboratory	y ot NKIVI



Job No. 4360/2

## **APPENDIX 4**

## CERTIFIED GEOTECHNICAL TEST RESULTS





Qty

27

21

1

2

1

## Contract Number: 40257

Client Ref: 4360/2 Client PO: 4360/2/CM

Laboratory Report

Report Date: 22-08-2018

Client Wilson Associates 36 Brunswick Road Gloucester GL1 1JJ

Contract Title: Cheltenham For the attention of: Tim Coe

Date Received: 07-08-2018 Date Commenced: 07-08-2018 Date Completed: 22-08-2018

#### **Test Description**

**Moisture Content** BS 1377:1990 - Part 2 : 3.2 - * UKAS

4 Point Liquid & Plastic Limit (LL/PL) BS 1377:1990 - Part 2 : 4.3 & 5.3 - * UKAS

Dry Den/MC (2.5kg Rammer Method 1 Litre Mould) BS 1377:1990 - Part 4 : 3.3 - * UKAS

Consolidated Drained Peak and Residual Shear Strength - set of 3 60 x 60mm Shear Box Specimens (5 days) BS1377 : 1990 Part 7 : 4 - * UKAS

Disposal of samples for job

Notes: Observations and Interpretations are outside the UKAS Accreditation

- * denotes test included in laboratory scope of accreditation
- # denotes test carried out by approved contractor
- @ denotes non accredited tests

This certificate is issued in accordance with the accreditation requirements of the United Kingdom Accreditation Service. The results reported herein relate only to the material supplied to the laboratory. This certificate shall not be reproduced except in full, without the prior written approval of the laboratory.

Approved Signatories:

Alex Wynn (Associate Director) - Ben Sharp (Contracts Manager) - Emma Sharp (Office Manager) Paul Evans (Quality/Technical Manager) - Richard John (Advanced Testing Manager) - Sean Penn (Administrative/Accounts Assistant) Wayne Honey (Administrative/Quality Assistant)

GEO Site & Testing Services Ltd Unit 3-4, Heol Aur, Dafen Ind Estate, Dafen, Llanelli, Carmarthenshire SA14 8QN Tel: 01554 784040 Fax: 01554 784041 info@gstl.co.uk gstl.co.uk

GST	[

### LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX (BS 1377 : Part 2 : 1990 Method 5)

601	15		•	SCRIPTIONS							
Contract Number			40257								
Site Name			C	Cheltenham							
WS											
Window Sample	Sample Number	Sample Type	Depth (m)	Description	5						

Window Sample	Sample Number	Sample Type	Depth (m)		Descriptions
WS1	1	Dist	2.00	-	Brown slightly silty CLAY
WS1	1	Dist	3.50	-	Brown slightly silty CLAY
WS2	1	Dist	0.70	-	Brown slightly silty CLAY
WS2	1	Dist	1.00	-	Brown slightly silty CLAY
WS2	1	Dist	3.00	-	Brown slightly silty CLAY
WS3	1	Dist	0.50	-	Brown slightly silty CLAY
WS3	1	Dist	3.80	-	Brown slightly silty CLAY
WS4	1	Dist	1.50	-	Brown slightly silty CLAY
WS4	1	Dist	2.50	-	Brown slightly silty CLAY
WS5	1	Dist	0.50	-	Brown slightly silty CLAY
WS5	1	Dist	1.70	-	Brown slightly silty CLAY
WS7	1	Dist	1.50	-	Brown slightly silty CLAY
WS7	1	Dist	2.50	-	Brown slightly silty CLAY
WS8	1	Dist	0.50	-	Brown slightly silty CLAY
WS8	1	Dist	2.00	-	Brown slightly silty CLAY
WS9	1	Dist	1.30	-	Brown slightly silty CLAY
WS9	1	Dist	2.30	-	Brown slightly silty CLAY
WS10	1	Dist	0.50	-	Brown slightly silty CLAY
WS10	1	Dist	1.50	-	Brown slightly silty CLAY
WS11	1	Dist	0.75	-	Brown slightly silty CLAY
WS11	1	Dist	1.75	-	Brown slightly silty CLAY
				-	
				-	
				-	

Operators	Checked	21/08/2018	Richard John	R
RO/MH	Approved	22/08/2018	Ben Sharp	RES

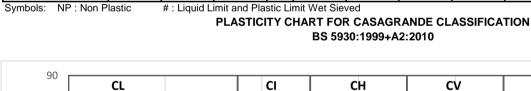


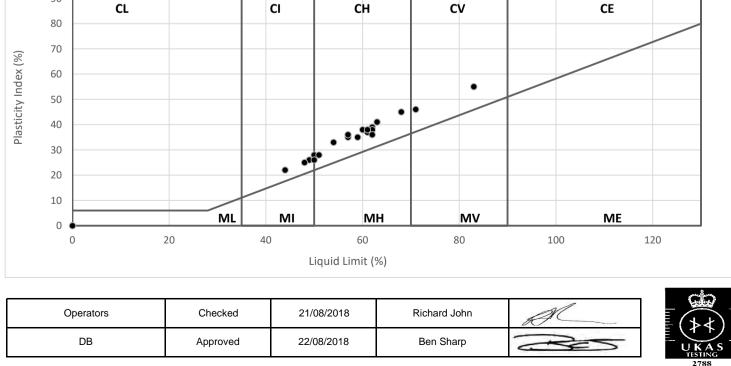


### LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX (BS 1377 : Part 2 : 1990 Method 5)

Contract Number	40257	
Site Name	Cheltenham	

WS Window Sample	Sample Number	Sample Type	D	epth (i	n)	Moisture Content %	Liquid Limit %	Plastic Limit %	Plasticity index %	Passing .425mm %	Remarks
WS1	1	Dist	2.00	-		26	62	23	39	100	CH High Plasticity
WS1	1	Dist	3.50	-		24	63	22	41	100	CH High Plasticity
WS2	1	Dist	0.70	-		25	83	28	55	100	CV Very High Plasticity
WS2	1	Dist	1.00	-		26	63	22	41	100	CH High Plasticity
WS2	1	Dist	3.00	-		27	60	22	38	100	CH High Plasticity
WS3	1	Dist	0.50	-		25	49	23	26	100	CI Intermediate Plasticity
WS3	1	Dist	3.80	-		22	62	24	38	100	CH High Plasticity
WS4	1	Dist	1.50	-		27	71	25	46	100	CV Very High Plasticity
WS4	1	Dist	2.50	-		25	61	24	37	100	CH High Plasticity
WS5	1	Dist	0.50	-		20	50	22	28	100	CI/H Inter/High Plasticity
WS5	1	Dist	1.70	-		22	61	23	38	100	CH High Plasticity
WS7	1	Dist	1.50	-		25	59	24	35	100	CH High Plasticity
WS7	1	Dist	2.50	-		20	57	22	35	100	CH High Plasticity
WS8	1	Dist	0.50	-		20	44	22	22	100	CI Intermediate Plasticity
WS8	1	Dist	2.00	-		22	57	21	36	100	CH High Plasticity
WS9	1	Dist	1.30	-		23	68	23	45	100	CH High Plasticity
WS9	1	Dist	2.30	-		21	62	26	36	100	CH High Plasticity
WS10	1	Dist	0.50	-		27	51	23	28	100	CH High Plasticity
WS10	1	Dist	1.50	-		23	50	24	26	100	CI/H Inter/High Plasticity
WS11	1	Dist	0.75	-		25	48	23	25	100	CI Intermediate Plasticity
WS11	1	Dist	1.75	-		18	54	21	33	100	CH High Plasticity
				-							
				-							





GSTL	LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX (BS 1377 : Part 2 : 1990 Method 5 ) DESCRIPTIONS	
Contract Number	40257	
Site Name	Cheltenham	

Hole Reference	Sample Number	Sample Type	Depth (m)		n)	Descriptions
6	1	Dist	0.50	-		Brown slightly silty CLAY
6	1	Dist	1.00	-		Brown slightly silty CLAY
6	1	Dist	1.50	-		Brown slightly silty CLAY
6	1	Dist	2.00	-		Brown slightly silty CLAY
6	1	Dist	2.50	-		Brown slightly silty CLAY
6	1	Dist	3.00	-		Brown slightly silty CLAY
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		
				-		

Operators	Checked	21/08/2018	Richard John	R
RO/MH	Approved	22/08/2018	Ben Sharp	R





DB

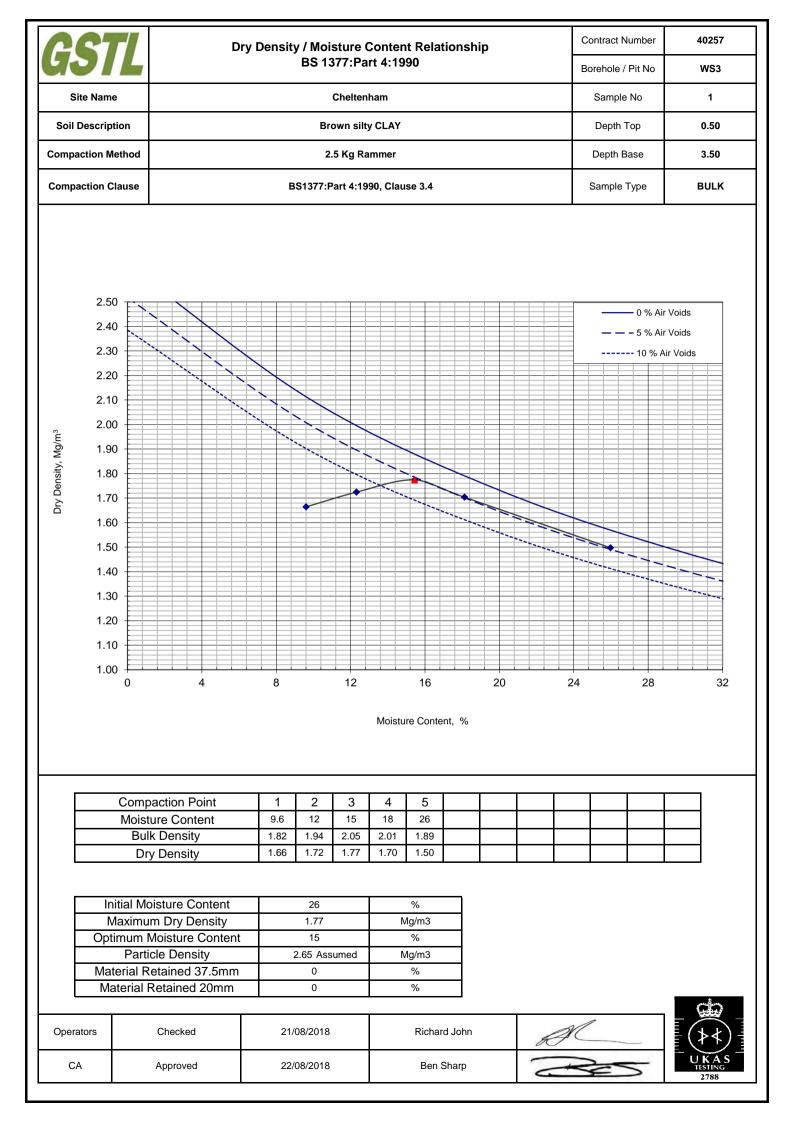
Approved

22/08/2018

Ben Sharp

## LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX

(BS 1377 : Part 2 : 1990 Method 5) Contract Number 40257 Site Name Cheltenham Passing Moisture Sample Sample Depth (m) Liquid Plastic Plasticity Remarks Content % 425mm % Hole Reference Number Limit % Limit % index % Туре Dist 0.50 21.7 1 6 -24.3 6 1 Dist 1.00 -6 1 Dist 1.50 -24.7 6 1 Dist 2.00 -19.3 Dist 1 2.50 18.8 6 -6 1 Dist 3.00 -19.5 ---------------Symbols: NP : Non Plastic # : Liquid Limit and Plastic Limit Wet Sieved PLASTICITY CHART FOR CASAGRANDE CLASSIFICATION BS 5930:1999+A2:2010 90 CL CI СН CV CE 80 70 Plasticity Index (%) 60 50 40 30 20 10 ML MI ΜН ΜV ME 0 0 20 40 60 80 100 120 Liquid Limit (%) 21/08/2018 Operators Checked Richard John

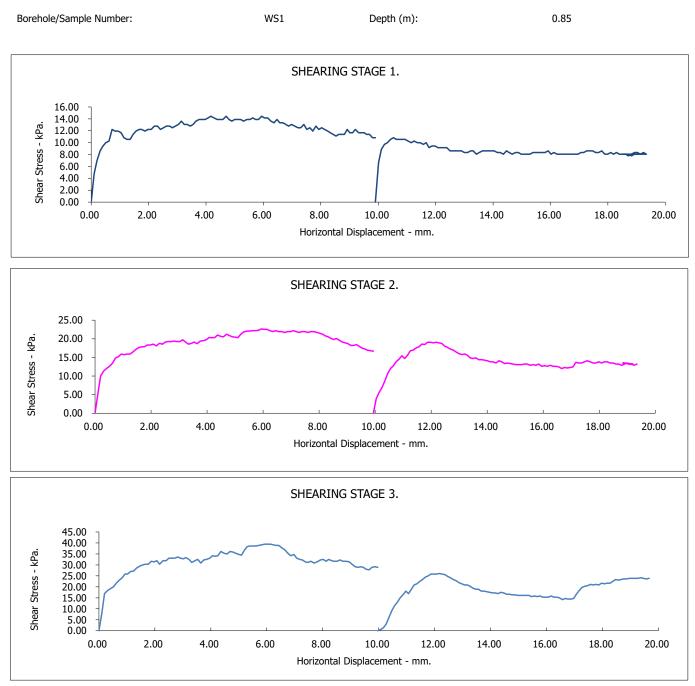


# **Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.** BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990

Borehole Number: Sample Number:		WS1		epth from (m): epth to (m):	0.85 0.00	
Sample Type:	D	Remould		g) material above 2.5		
Particle Density - Mg/m3:			2.65	(Assumed)		
Specimen Tested:		Submerg	jed			
Sample Description:						
Greyish brown slightly	silty CLAY				-	
STAGE Initial Conditions				1	2	3
Height - mm:				23.98	23.98	23.98
Length - mm:				60.00	60.00	60.00
Moisture Content - %:				19	19	19
Bulk Density - Mg/m3:				1.45	1.46	1.46
Dry Density - Mg/m3: Voids Ratio:				1.22	1.23	1.23
Normal Pressure- kPa				<u>1.1706</u> 25	1.1568 50	1.1568 100
Consolidation				25	50	100
Consolidated Height - mm	1:			22.78	21.79	20.79
Shear						
Rate of Strain (mm/min)				0.010		0.010
Strain at peak shear stres Peak shear Stress - kPa:	s (mm)			4.17 14	5.94	5.40
reak silear siless - kra.					23	55
PEAK	(0)					
Angle of Shearing Resista Effective Cohesion - kPa:	nce:( <del>0)</del>					18.5
RESIDUAL						0
Angle of Shearing Resista	nce:( <del>0)</del>					12.0
Effective Cohesion - kPa:						3
Shear Stress - (KPa).						
0	20	40	60 Normal Stress -(	80 kPa).	100	120
	•	Peak shear Stress - kPa:	Best	Fit Line ■	Residual shear Stress	
					DP Glass Checked Pages 1-4 by:	21/08/18 Date
					2 P Glans	21/08/18
					Approved Pages 1-4 by	Date
			Cheltenh	am		Contract No.: <b>40257</b> Client Ref Number: <b>4360/2</b>



# **Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.** BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990



Contract No.: 40257

Client Ref Number: 4360/2

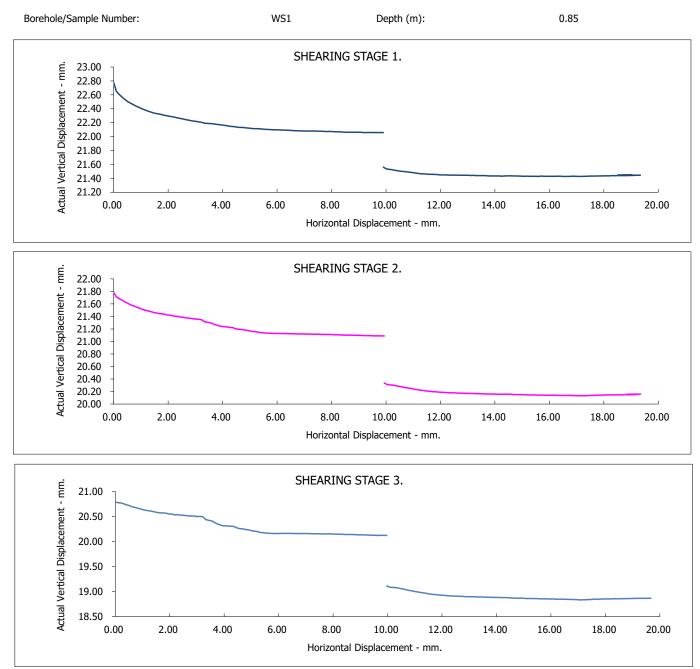
Cheltenham



04070405 CDP

### Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.

BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990



Contract No.: 40257

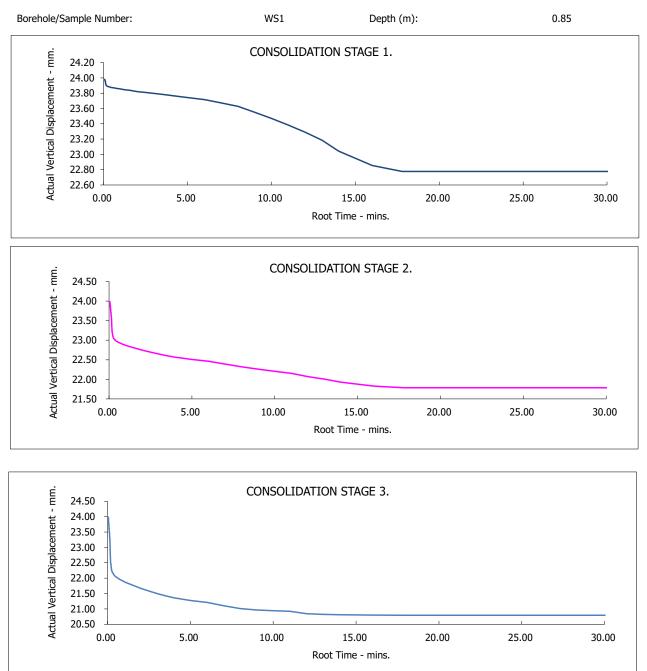
Cheltenham

Client Ref Number: 4360/2



## Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.

BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990



Contract No.: 40257

Client Ref Number: 4360/2

Cheltenham



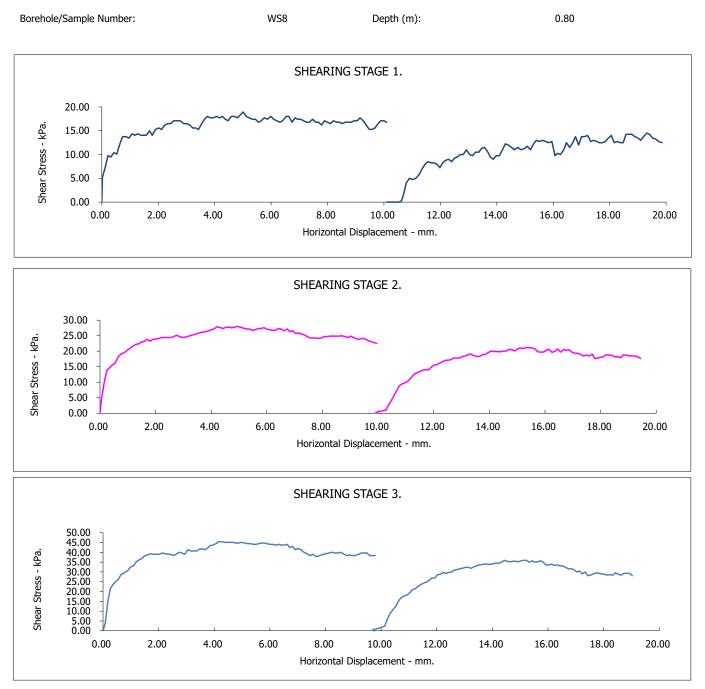
04070405 CDP

# **Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.** BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990

Borehole Number: Sample Number:		WS8	Depth from ( Depth to (m)	:	0.80 0.00	
Sample Type:	D	Remoulded (L	ight Tamping) material		nm removed	
Particle Density - Mg/m Specimen Tested:	3:	Submerged	2.65 (	Assumed)		
Sample Description: Greyish brown slight	lv silty CLAY					
STAGE	<i>,, .</i>		1		2	3
Initial Conditions				22.00	22.00	22.00
Height - mm: Length - mm:				23.98 60.00	23.98 60.00	23.98 60.00
Moisture Content - %:				14	14	14
Bulk Density - Mg/m3:				1.80	1.80	1.82
Dry Density - Mg/m3:				1.58	1.58	1.60
Voids Ratio: Normal Pressure- kPa				0.6730 25	0.6730	0.6581
Consolidation				25	50	100
Consolidated Height - m	ım:			23.33	22.34	21.36
Shear				0.010	0.010	0.010
Rate of Strain (mm/mir Strain at peak shear stra				0.010 5.01	0.010 4.94	0.010
Peak shear Stress - kPa				19	28	45
PEAK	toneo.(0)					10.0
Angle of Shearing Resis Effective Cohesion - kPa						<u>19.8</u> 10
RESIDUAL						10
Angle of Shearing Resis Effective Cohesion - kPa						15.8 7
Shear Stress - (KPa).						
0 0	20	40	60	80	100	120
		Norn	nal Stress -( kPa).			
		Peak shear Stress - kPa:	Best Fit Line		Residual shear Stress	
					DPGans Checked Pages 1-4 by: DPGans Approved Pages 1-4 by	21/08/18
		c	heltenham			Contract No.: 40257 Client Ref Number: 4360/2



# **Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.** BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990



Contract No.: 40257

Client Ref Number: 4360/2

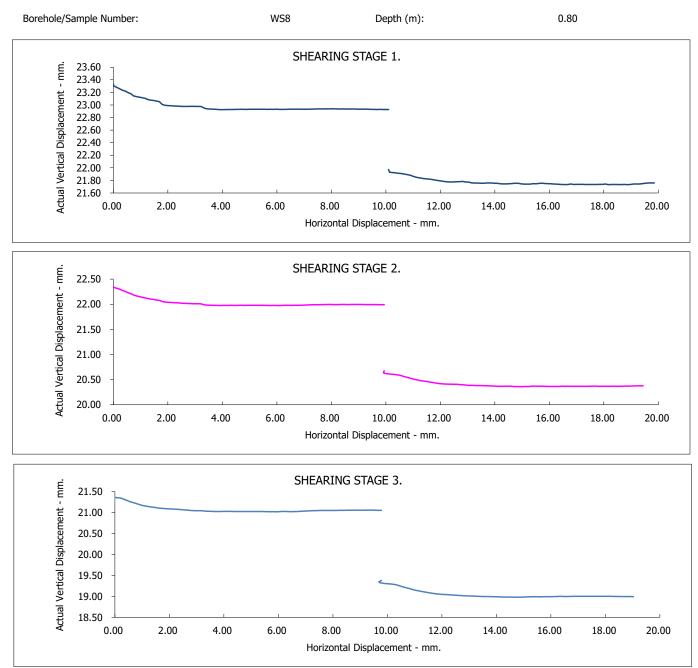
Cheltenham



04070405 CDP

### Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.

BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990



Contract No.: 40257

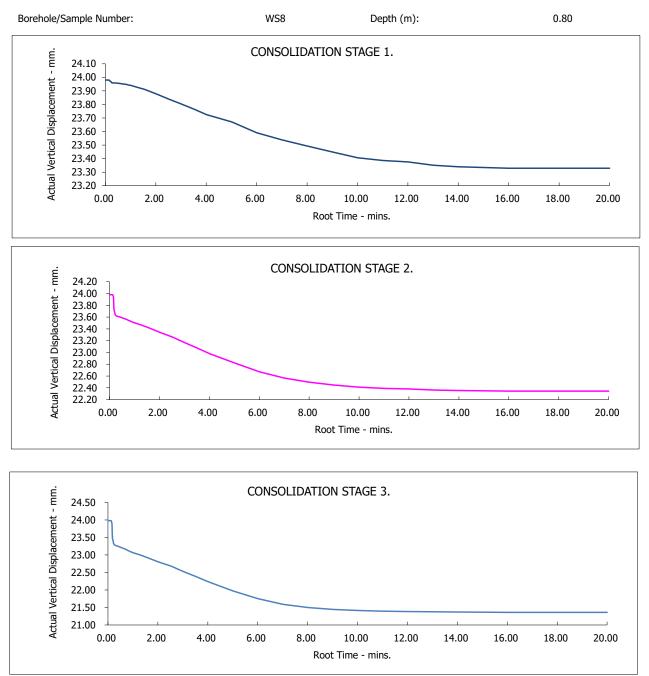
Cheltenham

Client Ref Number: 4360/2



## Test Report: CONSOLIDATED DRAINED PEAK AND RESIDUAL SHEARBOX TEST.

BS1377:Part 7.4.5.5 Shearing: multi-reversal test :1990



Contract No.: 40257

Client Ref Number: 4360/2

Cheltenham





Job No. 4360/2

## **APPENDIX** 5

## WASTE CLASSIFICATION REPORT AND CERTIFIED WASTE ACCEPTANCE CRITERIA (WAC) RESULTS



## Waste Classification Report



Job name				
Oakley Farm				
Description/Comments				
Project				
4360/2				
+300/2				
014				
Site				
Oakley Farm, Priors Road, Cheltenham				
Related Documents				
# Name		Description		
None				
Waste Stream Template				
Wilson Associates (Consulting) Limited				
Classified by				
	Com			
Name: <b>Tim Coe</b>		pany: <b>on Associates</b>		
Date:		runswick Road		
16 Nov 2018 14:08 GMT		icester		
Telephone:	GL1	1JJ		
01452422843				
Report				
Created by: Tim Coe Created date: 16 Nov 2018 14:08 GMT				
Job summary				
# Sample Name	Depth [m]	Classification Result	Hazard properties	Page
1 Sample 1		Non Hazardous		2
Appendices				Page
Appendix A: Classifier defined and non CL	P determinands			4
Appendix B: Rationale for selection of meta				5
Appendix C: Version				5



#### Classification of sample: Sample 1



#### Sample details

Sample Name: <b>Sample 1</b>	LoW Code: Chapter:	17: Construction and Demolition Wastes (including excavated soil
	Entry:	from contaminated sites) 17 05 04 (Soil and stones other than those mentioned in 17 05 03)

#### Hazard properties

None identified

#### **Determinands**

#### Moisture content: 0% Dry Weight Moisture Correction applied (MC)

#		Determinand CLP index number EC Number	CAS Number	CLP Note	User entered data	Conv. Factor	Compound conc.	Classification value	MC Applied	Conc. Not Used
1	-	arsenic { arsenic trioxide }	327-53-3		38 mg/kg	1.32	50.172 mg/kg	0.00502 %	∠	
2	4	cadmium { <mark>cadmium oxide</mark> }			1 mg/kg	1.142	1.142 mg/kg	0.000114 %	~	
	-		306-19-0	_					-	
3	4	oxide }			66 mg/kg	1.462	96.463 mg/kg	0.00965 %	$\checkmark$	
			308-38-9							
4	-		} 317-39-1		77 mg/kg	1.126	86.693 mg/kg	0.00867 %	$\checkmark$	
5	-	lead { lead chromate } 082-004-00-2 231-846-0 77	758-97-6	1	190 mg/kg	1.56	296.365 mg/kg	0.019 %	$\checkmark$	
6	4	mercury { mercury dichloride }			<1 mg/kg	1.353	<1.353 mg/kg	<0.000135 %		<lod< td=""></lod<>
-		080-010-00-X 231-299-8 74 nickel { nickel chromate }	487-94-7	_					Н	
7			4721-18-7		46 mg/kg	2.976	136.908 mg/kg	0.0137 %	$\checkmark$	
8	4	selenium { selenium compounds with the cadmium sulphoselenide and those spec in this Annex }			<3 mg/kg	2.554	<7.661 mg/kg	<0.000766 %		<lod< td=""></lod<>
	_	034-002-00-8								
9		zinc { zinc chromate } 024-007-00-3			190 mg/kg	2.774	527.088 mg/kg	0.0527 %	$\checkmark$	
10		рН	Ц		6.1 pH		6.1 pH	6.1 pH		
		naphthalene	11						H	
11		601-052-00-2 202-049-5 91	1-20-3		<0.1 mg/kg		<0.1 mg/kg	<0.00001 %		<lod< td=""></lod<>
12	0	acenaphthylene			<0.1 mg/kg	1	<0.1 mg/kg	<0.00001 %		<lod< td=""></lod<>
-		205-917-1 20 acenaphthene	08-96-8	_					H	
13	9	· ·	3-32-9		<0.1 mg/kg	1	<0.1 mg/kg	<0.00001 %		<lod< td=""></lod<>
14	8	fluorene 201-695-5 86	6-73-7		<0.1 mg/kg	1	<0.1 mg/kg	<0.00001 %		<lod< td=""></lod<>
15		phenanthrene	0-10-1		0.6 mg/kg	1	0.6 mg/kg	0.00006 %	1	
		201-581-5 85	5-01-8				5.5		Ÿ	



#			Determinand		CLP Note	User entered data	Conv. Factor	Compound conc.	Classification value	Applied	Conc. Not Used
		CLP index number	EC Number	CAS Number	CLP					MC	
16		anthracene	•	· ·		0.2 mg/kg		0.2 mg/kg	0.00002 %	$\checkmark$	
10			204-371-1	120-12-7		0.2 119/89		0.2 119/89	0.00002 /8	~	
17		fluoranthene				1 mg/kg		1 mg/kg	0.0001 %	$\checkmark$	
<u> </u>			205-912-4	206-44-0					0.0001 /0	~	
18		pyrene				0.9 mg/kg		0.9 mg/kg	0.00009 %	$\checkmark$	
			204-927-3	129-00-0					0.00000 /0	Ŷ	
19		benzo[a]anthracer	e			0.4 mg/kg		0.4 mg/kg	0.00004 %	$\checkmark$	
		601-033-00-9	200-280-6	56-55-3						Ň	
20		chrysene				0.4 mg/kg		0.4 mg/kg	0.00004 %	$\checkmark$	
		601-048-00-0	205-923-4	218-01-9					0.0000170	Ň	
21		benzo[b]fluoranthe	ene			0.4 mg/kg		0.4 mg/kg	0.00004 %	$\checkmark$	
		601-034-00-4	205-911-9	205-99-2					0.0000170	Ň	
22		benzo[k]fluoranthe	ne			0.3 mg/kg		0.3 mg/kg	0.00003 %	$\checkmark$	
		601-036-00-5	205-916-6	207-08-9		0.0 mg/kg		0.0 mg/kg	0.00000 /0	~	
23	1	benzo[a]pyrene; be	enzo[def]chrysene			0.3 mg/kg		0.3 mg/kg	0.00003 %	$\checkmark$	
20		601-032-00-3	200-028-5	50-32-8	-	0.0 mg/kg		0.0 mg/kg	0.00000 /0	~	
24		indeno[123-cd]pyre	ene			0.2 mg/kg		0.2 mg/kg	0.00002 %	$\checkmark$	
24			205-893-2	193-39-5		0.2 mg/kg		0.2 mg/kg	0.00002 /8	~	
25		dibenz[a,h]anthrac	ene			<0.1 mg/kg		<0.1 mg/kg	<0.00001 %		<lod< td=""></lod<>
20		601-041-00-2	200-181-8	53-70-3		<0.1 mg/kg		<0.1 mg/ng	<0.00001 /0		
26		benzo[ghi]perylene	е			0.2 mg/kg		0.2 mg/kg	0.00002 %	$\checkmark$	
20			205-883-8	191-24-2		0.2 mg/kg		0.2 1119/102	0.00002 /8	~	
27		DDT (ISO); clofend 1,1,1-trichloro-2,2- dichlorodiphenyltri 602-045-00-7	bis(4-chloropheny			<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
$\rightarrow$	-		200-024-3	50-29-3	+				· · · · · · · · · · · · · · · · · · ·		
28		chlordane (ISO); 1,2,4,5,6,7,8,8-oct methanoindan			_	<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
_		602-047-00-8	200-349-0	57-74-9	$\vdash$					-	
		hexachlorocyclohe	-								
29		602-043-00-6	210-168-9, 200-401-2, 206-270-8, 206-271-3	58-89-9, 319-84-6, 319-85-7, 608-73-1		<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
30		dieldrin (ISO) 602-049-00-9	200-484-5	60-57-1		<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
31		endrin (ISO); 1,2,3,4,10,10-hexa octahydro-1,4:5,8-	achloro-6,7-epoxy- dimethanonaphtha	1,4,4a,5,6,7,8,8a- alene		<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
		602-051-00-X	200-775-7	72-20-8							
32		heptachlor (ISO); 1,4,5,6,7,8,8-hepta methanoindene				<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
_		602-046-00-2	200-962-3	76-44-8	-					-	
33		hexachlorobenzen		440 74 4		<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
_		602-065-00-6	204-273-9	118-74-1	-					-	
34		aldrin (ISO) 602-048-00-3	206-215-8	309-00-2		<0.01 mg/kg		<0.01 mg/kg	<0.000001 %		<lod< td=""></lod<>
		· · · · · · · · · · · · · · · · · · ·						Total	0.11 %		

ŀ	"	21/	
	10	∍y	

Key	
	User supplied data
	Determinand values ignored for classification, see column 'Conc. Not Used' for reason
	Determinand defined or amended by HazWasteOnline (see Appendix A)
4	Speciated Deteminand - Unless the Determinand is Note 1, the Conversion Factor is used to calculate the compound concentration
<lod< th=""><th>Below limit of detection</th></lod<>	Below limit of detection
OLD: Note 4	

CLP: Note 1  $\,$  Only the metal concentration has been used for classification



#### Appendix A: Classifier defined and non CLP determinands

• chromium(III) oxide (EC Number: 215-160-9, CAS Number: 1308-38-9)

Conversion factor: 1.462 Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 17 Jul 2015 Hazard Statements: Aquatic Chronic 1 H410, Aquatic Acute 1 H400, Repr. 1B H360FD, Skin Sens. 1 H317, Resp. Sens. 1 H334, Skin Irrit. 2 H315, STOT SE 3 H335, Eye Irrit. 2 H319, Acute Tox. 4 H302, Acute Tox. 4 H332

PH (CAS Number: PH)

Description/Comments: Appendix C4 Data source: WM3 1st Edition 2015 Data source date: 25 May 2015 Hazard Statements: None.

acenaphthylene (EC Number: 205-917-1, CAS Number: 208-96-8)

Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 17 Jul 2015 Hazard Statements: Skin Irrit. 2 H315, STOT SE 3 H335, Eye Irrit. 2 H319, Acute Tox. 1 H310, Acute Tox. 1 H330, Acute Tox. 4 H302

acenaphthene (EC Number: 201-469-6, CAS Number: 83-32-9)

Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 17 Jul 2015 Hazard Statements: Aquatic Chronic 2 H411, Aquatic Chronic 1 H410, Aquatic Acute 1 H400, Skin Irrit. 2 H315, STOT SE 3 H335, Eye Irrit. 2 H319

[•] fluorene (EC Number: 201-695-5, CAS Number: 86-73-7)

Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 06 Aug 2015 Hazard Statements: Aquatic Chronic 1 H410 , Aquatic Acute 1 H400

• phenanthrene (EC Number: 201-581-5, CAS Number: 85-01-8)

Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 06 Aug 2015 Hazard Statements: Skin Irrit. 2 H315, Aquatic Chronic 1 H410, Aquatic Acute 1 H400, Skin Sens. 1 H317, Carc. 2 H351, STOT SE 3 H335, Eye Irrit. 2 H319, Acute Tox. 4 H302

^a anthracene (EC Number: 204-371-1, CAS Number: 120-12-7)

Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 17 Jul 2015 Hazard Statements: Aquatic Chronic 1 H410 , Aquatic Acute 1 H400 , Skin Sens. 1 H317 , Skin Irrit. 2 H315 , STOT SE 3 H335 , Eye Irrit. 2 H319

• fluoranthene (EC Number: 205-912-4, CAS Number: 206-44-0)

Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 21 Aug 2015 Hazard Statements: Aquatic Chronic 1 H410 , Aquatic Acute 1 H400 , Acute Tox. 4 H302

[•] pyrene (EC Number: 204-927-3, CAS Number: 129-00-0)

Description/Comments: Data from C&L Inventory Database; SDS Sigma Aldrich 2014

Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database

Data source date: 21 Aug 2015

Hazard Statements: Aquatic Chronic 1 H410 , Aquatic Acute 1 H400 , STOT SE 3 H335 , Eye Irrit. 2 H319 , Skin Irrit. 2 H315



#### ^e indeno[123-cd]pyrene (EC Number: 205-893-2, CAS Number: 193-39-5)

Description/Comments: Data from C&L Inventory Database Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 06 Aug 2015 Hazard Statements: Carc. 2 H351

#### • benzo[ghi]perylene (EC Number: 205-883-8, CAS Number: 191-24-2)

Description/Comments: Data from C&L Inventory Database; SDS Sigma Aldrich 28/02/2015 Data source: http://echa.europa.eu/web/guest/information-on-chemicals/cl-inventory-database Data source date: 23 Jul 2015 Hazard Statements: Aquatic Chronic 1 H410 , Aquatic Acute 1 H400

#### Appendix B: Rationale for selection of metal species

#### arsenic {arsenic trioxide}

Reasonable case CLP species based on hazard statements/molecular weight and most common (stable) oxide of arsenic. Industrial sources include: smelting; main precursor to other arsenic compounds (edit as required)

#### cadmium {cadmium oxide}

Reasonable case CLP species based on hazard statements/molecular weight, very low solubility in water. Industrial sources include: electroplating baths, electrodes for storage batteries, catalysts, ceramic glazes, phosphors, pigments and nematocides. (edit as required) Worst case compounds in CLP: cadmium sulphate, chloride, fluoride & iodide not expected as either very soluble and/or compound's industrial usage not related to site history (edit as required)

#### chromium in chromium(III) compounds {chromium(III) oxide}

Reasonable case species based on hazard statements/molecular weight. Industrial sources include: tanning, pigment in paint, inks and glass (edit as required)

#### copper {dicopper oxide; copper (I) oxide}

Reasonable case CLP species based on hazard statements/molecular weight and insolubility in water. Industrial sources include: oxidised copper metal, brake pads, pigments, antifouling paints, fungicide. (edit as required) Worse case copper sulphate is very soluble and likely to have been leached away if ever present and/or not enough soluble sulphate detected. (edit as required)

#### lead {lead chromate}

Worst case CLP species based on hazard statements/molecular weight (edit as required)

#### mercury {mercury dichloride}

Worst case CLP species based on hazard statements/molecular weight (edit as required)

#### nickel {nickel chromate}

Worst case CLP species based on hazard statements/molecular weight (edit as required)

#### selenium (selenium compounds with the exception of cadmium sulphoselenide and those specified elsewhere in this Annex)

Harmonised group entry used as most reasonable case. Pigment cadmium sulphoselenide not likely to be present in this soil. No evidence for the other CLP entries: sodium selenite, nickel II selenite and nickel selenide, to be present in this soil. (edit as required)

#### zinc {zinc chromate}

Worst case CLP species based on hazard statements/molecular weight (edit as required)

#### **Appendix C: Version**

HazWasteOnline Classification Engine: WM3 1st Edition v1.1, May 2018 HazWasteOnline Classification Engine Version: 2018.306.3704.7580 (03 Nov 2018) HazWasteOnline Database: 2018.306.3704.7580 (03 Nov 2018)



This classification utilises the following guidance and legislation: WM3 v1.1 - Waste Classification - 1st Edition v1.1 - May 2018 CLP Regulation - Regulation 1272/2008/EC of 16 December 2008 1st ATP - Regulation 790/2009/EC of 10 August 2009 2nd ATP - Regulation 286/2011/EC of 10 March 2011 3rd ATP - Regulation 618/2012/EU of 10 July 2012 4th ATP - Regulation 487/2013/EU of 8 May 2013 Correction to 1st ATP - Regulation 758/2013/EU of 7 August 2013 5th ATP - Regulation 944/2013/EU of 2 October 2013 6th ATP - Regulation 605/2014/EU of 5 June 2014 WFD Annex III replacement - Regulation 1357/2014/EU of 18 December 2014 Revised List of Wastes 2014 - Decision 2014/955/EU of 18 December 2014 7th ATP - Regulation 2015/1221/EU of 24 July 2015 8th ATP - Regulation (EU) 2016/918 of 19 May 2016 9th ATP - Regulation (EU) 2016/1179 of 19 July 2016 10th ATP - Regulation (EU) 2017/776 of 4 May 2017 HP14 amendment - Regulation (EU) 2017/997 of 8 June 2017 13th ATP - Regulation (EU) 2018/1480 of 4 October 2018 POPs Regulation 2004 - Regulation 850/2004/EC of 29 April 2004 1st ATP to POPs Regulation - Regulation 756/2010/EU of 24 August 2010 2nd ATP to POPs Regulation - Regulation 757/2010/EU of 24 August 2010



Concept Life Sciences is a trading name of Concept Life Sciences Analytical & Development Services Limited registered in England and Wales (No 2514788)

## **Concept Life Sciences**

### **Certificate of Analysis**

Hadfield House Hadfield Street Combrook Manchester M16 9FE Tel : 0161 874 2400 Fax : 0161 874 2468

Report Number: 757158-1

Date of Report: 15-Aug-2018

Customer: Wilson Associates (Consulting) Limited 36 Brunswick Road Gloucester GL1 1JJ

Customer Contact: Mr Charlie Morton

Customer Job Reference: 4360/2 Customer Purchase Order: 4360/2/CM Customer Site Reference: Cheltenham Date Job Received at Concept: 03-Aug-2018 Date Analysis Started: 06-Aug-2018 Date Analysis Completed: 15-Aug-2018

The results reported relate to samples received in the laboratory and may not be representative of a whole batch.

Opinions and interpretations expressed herein are outside the scope of UKAS accreditation This report should not be reproduced except in full without the written approval of the laboratory

Tests covered by this certificate were conducted in accordance with Concept Life Sciences SOPs All results have been reviewed in accordance with Section 25 of the Concept Life Sciences, Analytical Services Quality Manual







Report checked and authorised by : Aleksandra Pacula Senior Customer Service Advisor Issued by : Aleksandra Pacula Senior Customer Service Advisor

> Page 1 of 10 757158-1

## Waste Acceptance Criteria

Customer Sample Reference :	West Wac
Our Sample Reference :	757158 001
Project Site :	Cheltenham
Customer Reference :	4360/2
Test Portion Mass (g) :	175
Empty Dish Weight :	0
Wet Sample in Dish Weight :	100
Sample in Dish @ 105C :	79.1
Date Sampled :	30-JUL-2018
Matrix Class :	Clay

	Result	Inert Waste Landfill	Stable non reactive	Hazardous V Landfil				
Determinand	Technique	LOD	Units	Symbol				
Acid Neutralising Capacity (pH 4)	Titration	2	Mol/kg	Ν	<2			
Acid Neutralising Capacity (pH 7)	Titration	2	Mol/kg	Ν	<2			
BTEX (Sum)	Calc	0.040	mg/kg	U	<0.040	6.0		
PCB EC7 (Sum)	Calc	0.007	mg/kg	U	<0.007	1.0		
Loss on Ignition	Grav	0.1	%	N	8.2			10.0
PAH (Sum)	Calc	1.6	mg/kg	N	<1.6	100.0		
рН	Probe			М	7.5		> 6.0	
Total Organic Carbon	OX/IR	0.1	%	Ν	0.8	3.0	5.0	6.0
Total Petroleum Hydrocarbons C10-C40 (Sum)	Calc	1	mg/kg	N	⁽¹³⁾ <1	500.0		

	Data for BS EN 12457-2 (10:1)	Result	Inert Waste Landfill	Stable non reactive	Hazardous Waste Landfill			
Determinand	Technique	LOD	Units	Symbol				•
Antimony	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.06	0.7	5.0
Arsenic	Calc WAC ICP/MS	0.0020	mg/kg	Ν	<0.0020	0.5	2.0	25.0
Barium	Calc WAC ICP/MS	0.010	mg/kg	Ν	0.17	20.0	100.0	300.0
Cadmium	Calc WAC ICP/MS	0.00020	mg/kg	N	<0.00020	0.04	1.0	5.0
Chloride	Calc (W)	10	mg/kg	Ν	230	800.0	15000.0	25000.0
Chromium	Calc WAC ICP/MS	0.010	mg/kg	Ν	<0.010	0.5	10.0	70.0
Copper	Calc WAC ICP/MS	0.0050	mg/kg	Ν	<0.0050	2.0	50.0	100.0
Dissolved Organic Carbon	Calc	10	mg/kg	N	23	500.0	800.0	1000.0
Fluoride	Calc (W)	0.50	mg/kg	N	4.3	10.0	150.0	500.0
Lead	Calc WAC ICP/MS	0.0030	mg/kg	N	<0.0030	0.5	10.0	50.0
Mercury	Calc WAC ICP/MS	0.00050	mg/kg	N	<0.00050	0.01	0.2	2.0
Molybdenum	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.5	10.0	30.0
Nickel	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.4	10.0	40.0
Phenols (Total-Mono)	Calc	1.0	mg/kg	N	<1.0	1.0		
Selenium	Calc WAC ICP/MS	0.0050	mg/kg	N	<0.0050	0.1	0.5	7.0
Sulphate	Calc (W)	5	mg/kg	N	6900	1000.0	20000.0	50000.0
Total Dissolved Solids	Calc	1000	mg/kg	N	8100	4000.0	60000.0	100000.0
Zinc	Calc WAC ICP/MS	0.020	mg/kg	N	<0.020	4.0	50.0	200.0

Following the recommendation from the Environment Agency (England and Wales)*, the leachate preparation in this report has been carried out to BS EN 12457-2 : One Stage batch test at a liquid to solid ratio of 10 I/kg. This is also compliant with Schedule 10 of the Environmental Permitting Regulations 2010.

Note : This is the minimum amount of testing which is required.

Further testing may be required if :

- evidence of immediately leachable parameters becomes available.

- evidence to indicate that the sample could be classified as hazardous under H1-H14 of the Waste(England and Wales) Regulations 2011(as amended) becomes available.

Acceptance of waste at landfill is always at the discretion of the Landfill Operator.

* Waste Sampling and Testing for Disposal at Landfill, EBPRI 11507B, Environment Agency (England and Wales) March 2013

As detailed in-Waste Classification. Guidance on the classification and assessment of waste. Technical Guidance WM3:

https://www.gov.uk/government/uploads/system/uploads/attachment_data/file/427077/LIT_10121.pdf

Landfill WAC analysis (specifically leaching test results) should not be used for hazardous waste classification purposes. This analysis is only applicable for hazardous waste landfill acceptance and does not give any indication as to whether a waste may be hazardous or non-hazardous.



## Waste Acceptance Criteria

Customer Sample Reference :	Cent Wac
Our Sample Reference :	757158 002
Project Site :	Cheltenham
Customer Reference :	4360/2
Wet Sample in Dish Weight :	100
Empty Dish Weight :	0
Test Portion Mass (g) :	175
Sample in Dish @ 105C :	82.4
Date Sampled :	30-JUL-2018
Matrix Class :	Clay

	Soil				Result	Inert Waste Landfill	Stable non reactive	Hazardous Waste Landfill
Determinand	Technique	LOD	Units	Symbol				
Acid Neutralising Capacity (pH 4)	Titration	2	Mol/kg	N	<2			
Acid Neutralising Capacity (pH 7)	Titration	2	Mol/kg	Ν	<2			
BTEX (Sum)	Calc	0.040	mg/kg	U	<0.040	6.0		
PCB EC7 (Sum)	Calc	0.007	mg/kg	U	<0.007	1.0		
Loss on Ignition	Grav	0.1	%	Ν	5.2			10.0
PAH (Sum)	Calc	1.6	mg/kg	N	<1.6	100.0		
pH	Probe			М	6.9		> 6.0	
Total Organic Carbon	OX/IR	0.1	%	Ν	0.3	3.0	5.0	6.0
Total Petroleum Hydrocarbons C10-C40 (Sum)	Calc	1	mg/kg	N	⁽¹³⁾ <1	500.0		

	Data for BS EN 12457-2 (10:1)		Result	Inert Waste Landfill	Stable non reactive	Hazardous Waste Landfill		
Determinand	Technique	LOD	Units	Symbol				•
Antimony	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.06	0.7	5.0
Arsenic	Calc WAC ICP/MS	0.0020	mg/kg	Ν	<0.0020	0.5	2.0	25.0
Barium	Calc WAC ICP/MS	0.010	mg/kg	Ν	<0.010	20.0	100.0	300.0
Cadmium	Calc WAC ICP/MS	0.00020	mg/kg	Ν	<0.00020	0.04	1.0	5.0
Chloride	Calc (W)	10	mg/kg	N	34	800.0	15000.0	25000.0
Chromium	Calc WAC ICP/MS	0.010	mg/kg	Ν	<0.010	0.5	10.0	70.0
Copper	Calc WAC ICP/MS	0.0050	mg/kg	Ν	<0.0050	2.0	50.0	100.0
Dissolved Organic Carbon	Calc	10	mg/kg	Ν	29	500.0	800.0	1000.0
Fluoride	Calc (W)	0.50	mg/kg	N	6.0	10.0	150.0	500.0
Lead	Calc WAC ICP/MS	0.0030	mg/kg	N	<0.0030	0.5	10.0	50.0
Mercury	Calc WAC ICP/MS	0.00050	mg/kg	N	<0.00050	0.01	0.2	2.0
Molybdenum	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.5	10.0	30.0
Nickel	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.4	10.0	40.0
Phenols (Total-Mono)	Calc	1.0	mg/kg	N	<1.0	1.0		
Selenium	Calc WAC ICP/MS	0.0050	mg/kg	N	<0.0050	0.1	0.5	7.0
Sulphate	Calc (W)	5	mg/kg	N	42	1000.0	20000.0	50000.0
Total Dissolved Solids	Calc	1000	mg/kg	N	<1000	4000.0	60000.0	100000.0
Zinc	Calc WAC ICP/MS	0.020	mg/kg	N	<0.020	4.0	50.0	200.0

Following the recommendation from the Environment Agency (England and Wales)*, the leachate preparation in this report has been carried out to BS EN 12457-2 : One Stage batch test at a liquid to solid ratio of 10 I/kg. This is also compliant with Schedule 10 of the Environmental Permitting Regulations 2010.

Note : This is the minimum amount of testing which is required.

Further testing may be required if :

- evidence of immediately leachable parameters becomes available.

- evidence to indicate that the sample could be classified as hazardous under H1-H14 of the Waste(England and Wales) Regulations 2011(as amended) becomes available.

Acceptance of waste at landfill is always at the discretion of the Landfill Operator.

* Waste Sampling and Testing for Disposal at Landfill, EBPRI 11507B, Environment Agency (England and Wales) March 2013

As detailed in-Waste Classification. Guidance on the classification and assessment of waste. Technical Guidance WM3:

https://www.gov.uk/government/uploads/system/uploads/attachment_data/file/427077/LIT_10121.pdf

Landfill WAC analysis (specifically leaching test results) should not be used for hazardous waste classification purposes. This analysis is only applicable for hazardous waste landfill acceptance and does not give any indication as to whether a waste may be hazardous or non-hazardous.



## Waste Acceptance Criteria

Customer Sample Reference :	East Wac
Our Sample Reference :	757158 003
Project Site :	Cheltenham
Customer Reference :	4360/2
Test Portion Mass (g) :	175
Sample in Dish @ 105C :	81.1
Wet Sample in Dish Weight :	100
Empty Dish Weight :	0
Date Sampled :	30-JUL-2018
Matrix Class :	Clay

	Result	Inert Waste Landfill	Stable non reactive	Hazardous W Landfill				
Determinand	Technique	LOD	Units	Symbol				
Acid Neutralising Capacity (pH 4)	Titration	2	Mol/kg	Ν	<2			
Acid Neutralising Capacity (pH 7)	Titration	2	Mol/kg	Ν	<2			
BTEX (Sum)	Calc	0.040	mg/kg	U	<0.040	6.0		
PCB EC7 (Sum)	Calc	0.007	mg/kg	U	<0.007	1.0		
Loss on Ignition	Grav	0.1	%	N	6.7			10.0
PAH (Sum)	Calc	1.6	mg/kg	N	<1.6	100.0		
рН	Probe			М	7.3		> 6.0	
Total Organic Carbon	OX/IR	0.1	%	N	0.4	3.0	5.0	6.0
Total Petroleum Hydrocarbons C10-C40 (Sum)	Calc	1	mg/kg	N	⁽¹³⁾ <1	500.0		

	Data for BS EN 12457-2 (10:1)	Result	Inert Waste Landfill	Stable non reactive	Hazardous Waste Landfill			
Determinand	Technique	LOD	Units	Symbol				
Antimony	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.06	0.7	5.0
Arsenic	Calc WAC ICP/MS	0.0020	mg/kg	N	<0.0020	0.5	2.0	25.0
Barium	Calc WAC ICP/MS	0.010	mg/kg	N	0.016	20.0	100.0	300.0
Cadmium	Calc WAC ICP/MS	0.00020	mg/kg	N	<0.00020	0.04	1.0	5.0
Chloride	Calc (W)	10	mg/kg	N	<10	800.0	15000.0	25000.0
Chromium	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.5	10.0	70.0
Copper	Calc WAC ICP/MS	0.0050	mg/kg	N	<0.0050	2.0	50.0	100.0
Dissolved Organic Carbon	Calc	10	mg/kg	N	30	500.0	800.0	1000.0
Fluoride	Calc (W)	0.50	mg/kg	N	9.5	10.0	150.0	500.0
Lead	Calc WAC ICP/MS	0.0030	mg/kg	N	<0.0030	0.5	10.0	50.0
Mercury	Calc WAC ICP/MS	0.00050	mg/kg	N	<0.00050	0.01	0.2	2.0
Molybdenum	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.5	10.0	30.0
Nickel	Calc WAC ICP/MS	0.010	mg/kg	N	<0.010	0.4	10.0	40.0
Phenols (Total-Mono)	Calc	1.0	mg/kg	N	<1.0	1.0		
Selenium	Calc WAC ICP/MS	0.0050	mg/kg	N	<0.0050	0.1	0.5	7.0
Sulphate	Calc (W)	5	mg/kg	N	7	1000.0	20000.0	50000.0
Total Dissolved Solids	Calc	1000	mg/kg	N	<1000	4000.0	60000.0	100000.0
Zinc	Calc WAC ICP/MS	0.020	mg/kg	N	<0.020	4.0	50.0	200.0

Following the recommendation from the Environment Agency (England and Wales)*, the leachate preparation in this report has been carried out to BS EN 12457-2 : One Stage batch test at a liquid to solid ratio of 10 I/kg. This is also compliant with Schedule 10 of the Environmental Permitting Regulations 2010.

Note : This is the minimum amount of testing which is required.

Further testing may be required if :

- evidence of immediately leachable parameters becomes available.

- evidence to indicate that the sample could be classified as hazardous under H1-H14 of the Waste(England and Wales) Regulations 2011(as amended) becomes available.

Acceptance of waste at landfill is always at the discretion of the Landfill Operator.

* Waste Sampling and Testing for Disposal at Landfill, EBPRI 11507B, Environment Agency (England and Wales) March 2013

As detailed in-Waste Classification. Guidance on the classification and assessment of waste. Technical Guidance WM3:

https://www.gov.uk/government/uploads/system/uploads/attachment_data/file/427077/LIT_10121.pdf

Landfill WAC analysis (specifically leaching test results) should not be used for hazardous waste classification purposes. This analysis is only applicable for hazardous waste landfill acceptance and does not give any indication as to whether a waste may be hazardous or non-hazardous.



Concept Reference:	757158									
Project Site:	Cheltenham									
Customer Reference:	4360/2									
Soil	Analysed as Soil									
MCERTS Preparation										
		Concept Reference 757158 001 757158 002 757158 00								
		Custor	ner Sample	e Reference	West Wac	Cent Wac	East Wac			
			1	Fest Sample	AR	AR	AR			
			Da	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018			
			N	Matrix Class	Clay	Clay	Clay			
Determinand	Method	LOD	Units	Symbol						
Moisture @105C	Grav (1 Dec) (105 C)	0.1	%	Ν	21	18	19			

Concept Reference:	757158						
Project Site:	Cheltenham						
Customer Reference:	4360/2						
Soil	Analysed as	Soil					
MCERTS Preparation							
			Concep	ot Reference	757158 001	757158 002	757158 003
		Custo		e Reference		Cent Wac	757158 003 East Wac
		Custo	mer Sampl		West Wac		
		Custo	mer Sampl -	e Reference	West Wac M40	Cent Wac	East Wac
		Custo	mer Sampl - Da	e Reference Test Sample	West Wac M40 30-JUL-2018	Cent Wac M40	East Wac M40
Determinand	Method	Custo	mer Sampl - Da	le Reference Test Sample ate Sampled	West Wac M40 30-JUL-2018	Cent Wac M40 30-JUL-2018	East Wac M40 30-JUL-2018

Concept Reference: 757158 Project Site: Cheltenham

Customer Referen	<b>ce:</b> 4360/2						
Soil	Analysed as Soil						
втех							
			Concep	t Reference	757158 001	757158 002	757158 003
		Custor	ner Sampl	e Reference	West Wac	Cent Wac	East Wac
			1	Test Sample	M105	M105	M105
		25	Da	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018
				Matrix Class	Clay	Clay	Clay
Determinand	Method	LOD	Units	Symbol			
Benzene	GC/MS (Head Space)(MCERTS)	10	µg/kg	М	⁽¹³⁾ <10	⁽¹³⁾ <10	⁽¹³⁾ <10
Toluene	GC/MS (Head Space)(MCERTS)	10	µg/kg	М	<10	<10	<10
EthylBenzene	GC/MS (Head Space)(MCERTS)	10	µg/kg	М	<10	<10	<10
Meta/Para-Xylene	GC/MS (Head Space)(MCERTS)	10	µg/kg	М	<10	<10	<10
Ortho-Xylene	GC/MS (Head Space)(MCERTS)	10	µg/kg	М	<10	<10	<10

Concept Reference:	757158							
Project Site:	Chelten	ham						
Customer Reference:	4360/2							
Soil	Analyse	d as Soil						
PCB EC7 and Total								
				Concep	t Reference	757158 001	757158 002	757158 003
			Custo	mer Sample	e Reference	West Wac	Cent Wac	East Wac
				٦	est Sample	AR	AR	AR
				Da	te Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018
				I	Aatrix Class	Clay	Clay	Clay
Determinand		Method	LOD	Units	Symbol			
Polychlorinated biphenyl BZ	Z#28	GC/MS (SIR)	1	µg/kg	U	<1	<1	<1
Polychlorinated biphenyl BZ	Z#52	GC/MS (SIR)	1	µg/kg	U	<1	<1	<1
Polychlorinated biphenyl BZ	Z#101	GC/MS (SIR)	1	µg/kg	U	<1	<1	<1
Polychlorinated biphenyl BZ	Z#118	GC/MS (SIR)	1	µg/kg	U	<1	<1	<1
Polychlorinated biphenyl BZ	Z#138	GC/MS (SIR)	1	µg/kg	U	<1	<1	<1
Polychlorinated biphenyl BZ	Z#153	GC/MS (SIR)	1	µg/kg	U	<1	<1	<1
Polychlorinated biphenyl BZ	Z#180	GC/MS (SIR)	1	µg/kg	U	<1	<1	<1

#### Concept Reference: 757158 Project Site: Cheltenham Customer Reference: 4360/2

Soil Analysed as Soil

Total and Speciated USEPA16 PAH, Coronene & Phenol

			Concep	t Reference	757158 001	757158 002	757158 003
		Custo	mer Sampl	e Reference	West Wac	Cent Wac	East Wac
			1	Fest Sample	M105	M105	M105
			Da	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018
		Matrix Class	Clay	Clay	Clay		
Determinand	Method	LOD	Units	Symbol			
Naphthalene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Acenaphthylene	GC/MS (MCERTS)	0.1	mg/kg	U	<0.1	<0.1	<0.1
Acenaphthene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Fluorene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Phenanthrene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Anthracene	GC/MS (MCERTS)	0.1	mg/kg	U	<0.1	<0.1	<0.1
Fluoranthene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Pyrene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Benzo(a)Anthracene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Chrysene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Benzo(b/k)Fluoranthene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Benzo(a)Pyrene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Indeno(123-cd)Pyrene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Dibenzo(ah)Anthracene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Benzo(ghi)Perylene	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Polyaromatic Hydrocarbons (Total)	GC/MS (MCERTS)	0.1	mg/kg	U	<0.1	<0.1	<0.1
Phenol	GC/MS (MCERTS)	0.1	mg/kg	М	<0.1	<0.1	<0.1
Coronene	GC/MS	0.1	mg/kg	N	<0.1	<0.1	<0.1

Concept Reference:	757158	- 200		a second				
Project Site:	Cheltenham							
Customer Reference:	4360/2							
Soil	Analysed as Soil							
ТРН								
			-	Conce	ot Reference	757158 001	757158 002	757158 003
			Custor	ner Sampl	e Reference	West Wac	Cent Wac	East Wac
					Test Sample	M105	M105	M105
				D	ate Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018
					Matrix Class	Clay	Clay	Clay
Determinar	nd	Method	LOD	Units	Symbol			
Total Petroleum Hydrocarb	ons	GC/FID	1	mg/kg	М	(13) <1	⁽¹³⁾ <1	⁽¹³⁾ <1
Total Petroleum Hydrocarb	ons (C35-C40)	GC/FID	1	mg/kg	N	(13) <1	⁽¹³⁾ <1	⁽¹³⁾ <1

Concept Reference:	757158						
Project Site:	Cheltenham						
Customer Reference:	4360/2						
Leachate to BS EN 12457-2 (10:1)	Analysed as Water						
Waste Acceptance Criteri	а						
			Concep	t Reference	757158 001	757158 002	757158 003
		Custor	ner Sample	e Reference	West Wac	Cent Wac	East Wac
			I	est Sample	10:1	10:1	10:1
			Da	te Sampled	30-JUL-2018	30-JUL-2018	30-JUL-2018
			N	Aatrix Class	Clay	Clay	Clay
Determinand	Method	LOD	Units	Symbol			
Arsenic (Dissolved)	ICP/MS (Filtered)	0.2	µg/l	U	<0.2	<0.2	<0.2
Barium (Dissolved)	ICP/MS (Filtered)	1	µg/l	U	17	<1	2
Molybdenum (Dissolved)	ICP/MS (Filtered)	1	µg/l	Ν	<1	<1	<1
Total Dissolved Solids	Grav	100	mg/l	Ν	810	<100	<100
Phenols (Total-Mono)	Colorimetry	0.1	mg/l	U	<0.1	<0.1	<0.1
Dissolved Organic Carbon	OX/IR	1	mg/l	Ν	2	3	3
Electrical Conductivity	Probe	10	µS/cm	Ν	1400	70	150
Antimony (Dissolved)	ICP/MS (Filtered)	1	µg/l	U	<1	<1	<1
Cadmium (Dissolved)	ICP/MS (Filtered)	0.02	µg/l	U	<0.02	<0.02	<0.02
Chromium (Dissolved)	ICP/MS (Filtered)	1	µg/l	U	<1	<1	<1
Copper (Dissolved)	ICP/MS (Filtered)	0.5	µg/l	U	<0.5	<0.5	<0.5
Lead (Dissolved)	ICP/MS (Filtered)	0.3	µg/l	U	<0.3	<0.3	<0.3
Mercury (Dissolved)	ICP/MS (Filtered)	0.05	µg/l	U	<0.05	<0.05	<0.05
Nickel (Dissolved)	ICP/MS (Filtered)	1	µg/l	U	<1	<1	<1
Selenium (Dissolved)	ICP/MS (Filtered)	0.5	µg/l	U	<0.5	<0.5	<0.5
Zinc (Dissolved)	ICP/MS (Filtered)	2	µg/l	U	<2	<2	<2
Chloride	Discrete Analyser	1	mg/l	U	23	3	<1
Fluoride	Discrete Analyser	0.05	mg/l	U	0.43	0.60	0.95
Sulphate	Discrete Analyser	0.5	mg/l	U	690	4.2	0.7

## Index to symbols used in 757158-1

Value	Description
10:1	Leachate to BS EN 12457-2 (10:1)
A40	Assisted dried < 40C
M105	Analysis conducted on an "as received" aliquot. Results are reported on a dry weight basis where moisture content was determined by assisted drying of sample at 105C
M40	Analysis conducted on sample assisted dried at no more than 40C. Results are reported on a dry weight basis.
10:1 S	Data for BS EN 12457-2 (10:1)
AR	As Received
13	Results have been blank corrected.
М	Analysis is MCERTS accredited
U	Analysis is UKAS accredited
Ν	Analysis is not UKAS accredited

#### Notes

These samples have been analysed exceeding recommended holding times for PCB. It is possible therefore that the results provided may be compromised.



Job No. 4360/2

## **APPENDIX** 6

## GAS/WATER MONITORING RESULTS



### Monitoring undertaken 17 August 2018

Atmospheric Pressure	Temperature (°C)	BH No	C	Concentrations (%	)	Flow rates (l/hr)	Standing water	Depth and horizon of
(mb) and Trend	and Weather		CH₄	CO ₂	O ₂		level (m, bgl)	response zone (m,bgl)
1013		WS1	0.0	1.7	19.3	-0.1/-0.0	3.76	1.0 - 4.0
1010		WS2	0.0	0.6	20.0	-0.0/+0.0	3.46	1.0 - 4.0
1010		WS3					3.64	1.0 - 4.0
1012	16 - 17º C	WS4	0.0	5.3	16.6	-0.0/+0.0	3.48	1.0 - 4.0
	Fair	WS6	0.0	1.5	19.6	+0.0/+0.0	3.38	1.0 - 4.0
1010		WS8					1.05	1.0 - 4.0
		WS10					1.53	1.0 - 4.0
1008		WS11	0.0	1.4	20.1	+0.0/+0.1	1.65	1.0 - 4.0

Subcontracted to CC Ground Investigations

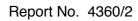
Gas monitoring carried out using a GA5000 Gas Analyser

Water monitoring carried out using a Geotechnical Instruments Dip Meter



### Monitoring undertaken 24 August 2018

Atmospheric Pressure	Temperature (°C)	BH No	Time (secs/ mins)	Cor	centrations	8 (%)	Flow rates time	Flow rates	Standing water	Depth and horizon of
(mb) and Trend	and Weather			CH₄	CO2	O2	(secs/mins)	(l/hr)	level (m, bgl)	response zone (m,bgl)
1005	14° C	WS1	15s	0.0	1.6	20.2	15s	0.0	3.76	1.0 - 4.0
	Cloudy /		30s	0.0	1.6	19.9	30s	0.0		
	sunny		45s	0.0	1.6	19.9	45s	0.0		
			1m	0.0	1.6	19.9	1m	0.0		
			2m	0.0	1.6	19.9	2m	0.0		
			3m	0.0	1.6	19.9	3m	-0.1		
			4m	0.0	1.6	19.8	4m	-0.1		
			5m	0.0	1.5	19.8	5m	-0.1		
			Max Peak	0.0	1.6		Max Peak	0.0		
			Steady Values	0.0	1.6		Steady Values	0.0		
1004	14° C	WS2	15s	0.0	0.5	20.4	15s	0.0	3.26	1.0 – 4.0
	Cloudy /		30s	0.0	0.5	20.3	30s	0.0		
	sunny		45s	0.0	0.5	20.3	45s	0.0		
			1m	0.0	0.5	20.3	1m	0.0		
			2m	0.0	0.5	20.3	2m	0.0		
			3m	0.0	0.5	20.3	3m	-0.1		
			4m	0.0	0.5	20.3	4m	0.0		
			5m	0.0	0.5	20.3	5m	-0.1		
			Max Peak	0.0	0.5		Max Peak	0.0		
			Steady Values	0.0	0.5		Steady Values	0.0		
	14° C									
1004	Cloudy / sunny	WS3							3.47	1.0 - 4.0
1004	15° C	WS4	15s	0.0	2.5	19.2	15s	0.0	3.26	1.0 - 4.0
	Light cloud /		30s	0.0	3.6	18.3	30s	-0.1		
	sunny		45s	0.0	4.3	17.9	45s	-0.1		
			1m	0.0	4.7	17.7	1m	-0.1		
			2m	0.0	4.9	17.6	2m	0.0		
			3m	0.0	4.9	17.6	3m	0.0		
			4m	0.0	4.9	17.6	4m	0.0		
			5m	0.0	4.6	17.8	5m	0.0		
			6m	0.0	4.2	18.0	6m			
			7m	0.0	3.8	18.4	7m			
			8m	0.0	3.5	18.6	8m			
			9m	0.0	3.2	18.9	9m			
			10m	0.0	3.0	19.0	10m		1	
			Max Peak	0.0	4.9		Max Peak	0.0		
			Steady Values	0.0			Steady Values	0.0		





Atmospheric Pressure	Temperature (°C)	BH No	Time (secs/ mins)	Cor	ncentrations	8 (%)	Flow rates time	Flow rates	Standing water	Depth and horizon of
(mb) and Trend	and Weather			CH₄	CO2	O ₂	(secs/mins)	(l/hr)	level (m, bgl)	response zone (m,bgl)
1002	15° C	WS6	15s	0.0	1.5	20.4	15s	0.0	3.13	1.0 – 4.0
	Cloudy		30s	0.0	1.5	20.2	30s	0.0		
			45s	0.0	1.5	20.0	45s	0.0		
			1m	0.0	1.5	20.0	1m	0.0		
			2m	0.0	1.5	20.0	2m	0.0		
			3m	0.0	1.5	20.0	3m	0.0		
			4m	0.0	1.5	20.0	4m	0.0		
			5m	0.0	1.5	20.0	5m	0.0		
			Max Peak	0.0	1.5		Max Peak	0.0		
			Steady Values	0.0	1.5		Steady Values	0.0		
	15° C Cloudy	WS8							1.02	1.0 – 4.0
	15° C Cloudy	WS10							1.48	1.0 – 3.0
1002	15° C	WS11	15s	0.0	1.3	20.5	15s	0.0	1.68	1.0 – 4.0
	Cloudy		30s	0.0	1.3	20.1	30s	0.0		
			45s	0.0	1.3	20.1	45s	0.0		
			1m	0.0	1.3	20.1	1m	0.0		
			2m	0.0	1.3	20.0	2m	0.0		
			3m	0.0	1.3	20.0	3m	0.0		
			4m	0.0	1.3	20.0	4m	0.0		
			5m	0.0	1.3	20.0	5m	0.0		
			Max Peak	0.0	1.3		Max Peak	0.0		
			Steady Values	0.0	1.3		Steady Values	0.0		

Monitoring undertaken by Wilson Associates Consulting Limited Gas monitoring carried out using a GA5000 Gas Analyser Water monitoring carried out using a Geotechnical Instruments Dip Meter



### Monitoring undertaken 18 September 2018

Atmospheric Pressure	Temperature (°C)	BH No	(	Concentrations (%	)	Flow rates (min / max)	Standing water	Depth and horizon of
(mb) and Trend	and Weather		CH₄	CO2	O ₂	(l/hr)	level (m, bgl)	response zone (m,bgl)
1000		WS1	0.0	0.9	20.3	+0.1/+0.2	3.52	1.0 - 4.0
		WS2	0.0	0.3	20.6	+0.0/+0.0	2.61	1.0 – 4.0
999		WS3					3.01	1.0 – 4.0
999	16 - 17º C	WS4	0.0	3.8	18.5	+0.0/+0.1	2.62	1.0 – 4.0
	Cloudy with gusts of wind	WS6	0.0	1.1	20.2	+0.0/+0.1	2.81	1.0 – 4.0
998		WS8					1.12	1.0 – 4.0
		WS10					1.53	1.0 – 3.0
996		WS11	0.0	1.0	20.3	+0.0/+0.1	1.68	1.0 - 4.0

Subcontracted to CC Ground Investigations

Gas monitoring carried out using a GA5000 Gas Analyser

Water monitoring carried out using a Geotechnical Instruments Dip Meter

# **SERVICE REPORT**





Date Of Calibration: 02-Jul-2018

Certificate Number: G501432_2/20881

#### ISSUED BY: GEOTECHNICAL INSTRUMENTS (UK) LTD

Wilson Associates (Consulting) Ltd
36 Brunswick Road GLOUCESTER Gloucestershire GL1 1JJ UNITED KINGDOM
Gas Analyser
GA5000
G501432

#### **UKAS Accredited results:**

Results after adjustment :

Methane (CH₄)				
Certified Gas (%)	Instrument Reading (%)	Uncertainty (%)		
5.0	4.9	0.41		
15.0	14.9	0.64		
50.0	49.3	0.94		

Carbon Dioxide (CO ₂ )				
Certified Gas (%)	Instrument Reading (%)	Uncertainty (%)		
5.0	4.8	0.43		
15.0	14.7	0.70		
50.0	49.8	1.1		

Oxygen (O ₂ )				
Certified Gas (%)	Instrument Reading (%)	Uncertainty (%)		
21.0	21.0	0.31		

The inwards assessment was carried out 15-Jun-2018.

The maximum adjustment was less than the inwards assessment uncertainty.

Inwards assessment data is available if requested.

All concentrations are molar.

$CH_4$ , $CO_2$ readings recorded at :	35.5 °C ± 2.5 °C
O2 readings recorded at :	23.8 °C ± 2.5 °C
Barometric Pressure :	1011 mbar ± 4 mbar

Method of Test : The analyser is calibrated in a temperature controlled chamber using a series of reference gases, in compliance with procedure LP004.



Sovereign House, Queensway, Learnington Spa, Warwickshire, CV31 3JR







Certificate Number: G501432_2/20881

Date Of Calibration: 02-Jul-2018

ISSUED BY: GEOTECHNICAL INSTRUMENTS (UK) LTD

The reported expanded uncertainty is based on a standard uncertainty multiplied by a coverage factor of k=2, providing a level of confidence of approximately 95%. The uncertainty evaluation has been carried out in accordance with UKAS requirements.

Calibrations marked 'Non-UKAS Accredited results' on this certificate have been included for completeness.

#### Non-UKAS accredited results after adjustment:

Barom	eter (mbar)
Reference	Instrument Reading
1011	1011

Internal Flow				
Applied (l/hr)	Instrument Reading (I/hr)			
5.0	5.1			
10.0	10.1			

Date of Issue : 03-Jul-2018

Approved by Signatory

'é

Dawn Hemings

Laboratory Inspection

